

RESEARCH AND EDUCATION

## Retention force and deformation of an innovative attachment model for mini-implant–retained overdentures



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Complete edentulism still affects a large portion of the world's population.<sup>1</sup> A conventional complete denture is commonly provided to restore masticatory function and esthetics; however, complete denture stability is limited in patients with marked bone resorption, especially mandibular resorption.<sup>1,2</sup> Implant-retained overdentures are an excellent alternative for these patients because of improved masticatory efficiency, comfort, and patient satisfaction.<sup>3-6</sup>

The use of implants to support a prosthesis has significant advantages in restoring physiological functions. According to the McGill consensus,<sup>7</sup> the installation of 2 conventional implants is considered the standard treatment for edentulous mandibles.<sup>8,9</sup> However, lack of bone, systemic or psychological problems, or financial conditions may limit the placement of implants. For these patients, mini-implant-retained overdentures may be a viable treatment option.<sup>10,11</sup> Some authorities propose using 4<sup>12,13</sup> mini-implants, and others suggest using only 2<sup>10,14-16</sup> for overdenture retention because the authors consider that reducing the number of mini-implants reduces cost and is more favorable biomechanically.

### ABSTRACT

**Statement of problem.** The gradual loss of retention and the need for periodic replacement of attachment-system components are the most frequent complications in implant-supported overdentures.

**Purpose.** The purpose of this in vitro study was to develop a new attachment system for overdentures with polymeric materials and compare its retention and deformation with a conventional O-ring attachment system.

**Material and methods.** A matrix with 2 mini-implants with ball abutments was used to simulate the mandibular border during a fatigue resistance test. A total of 60 polyacetal (n=20), polytetrafluoroethylene (n=20), and conventional O-ring (n=20) attachments were captured in pairs with acrylic resin and subjected to 3625 insertion and removal cycles, simulating 30 months of overdenture use. The internal and external deformations of the attachments were assessed using an optical stereomicroscope. One-way ANOVA and the Tukey honestly significant difference tests were used for statistical evaluation ( $\alpha=.05$ ).

**Results.** The polyacetal attachment system showed the highest retention ( $P<.001$ ), followed by the O-ring and polytetrafluoroethylene attachments. The O-ring attachments exhibited the lowest deformation ( $P<.001$ ), and the polyacetal attachments had the highest internal deformation ( $P<.001$ ).

**Conclusions.** The newly developed polyacetal attachment model increased the retention of mini-implant–retained overdentures, and despite the deformation experienced, the retention period appears to be better than that of conventional systems. (*J Prosthet Dent* 2019;121:129-34)

Many mini-implants are manufactured with ball abutments (Intra-Lock International Inc). This is financially advantageous over standard implants requiring a specific retention system for prostheses, including O-ring, ERA, or clip systems.<sup>1</sup> The system of choice for mini-implant-retained overdentures is the ball/O-ring attachment.<sup>1,11,14,17</sup> These attachments enable movement in different directions; are easily inserted, removed, cleaned, and maintained; and are affordable.<sup>2,18</sup>

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## Clinical Implications

The need for periodic replacement of the O-ring attachments is one of the major problems with implant-retained overdentures. Thus, the use of systems with longer durability provides better quality of treatment and patient satisfaction.

The gradual loss of retention and need for periodic change<sup>19,20</sup> are among the disadvantages of O-rings, especially in nonparallel implants,<sup>2,18,21,22</sup> compromising the biomechanics and success of implant-retained overdentures.<sup>23,24</sup> Although the authors are unaware of studies specifying a minimum retention value for mini-implants,<sup>11-13,25</sup> an optimal attachment system should provide sufficient resistance to vertical displacement and impart low lateral force to the implant during prosthesis insertion and removal.<sup>26</sup>

The solution to the problem of retention loss and O-ring wear is the development of devices with variable retention and the ability to take full advantage of the mechanical properties of each material.<sup>27,28</sup> Therefore, this in vitro study tested a new overdenture attachment using polymeric materials and compared the retention and deformation forces of these materials with those of a commercially available O-ring model. The null hypothesis tested was that the different attachments tested for mini-implant-retained overdentures would have no effect on the retention force and component deformation.

## MATERIAL AND METHODS

A polyurethane resin matrix (20×10×30 mm) (F16 Polyol; Axson) with 2 mini-implants (2.0×10.0 mm) (MDL; Intra-Lock International Inc) was used to simulate implants placed in the mandible. The implants were 25 mm apart and parallel to each other (Fig. 1).

A total of 40 polymeric attachments measuring 4×3 mm in height (Fig. 2) were developed using polytetrafluoroethylene (PTFE) (n=20) and polyacetal (n=20). The control group consisted of 20 metallic attachments with silicone O-rings (DML; Intra-Lock International Inc).

The recommended O-ring position is determined by the ideal path of insertion, perpendicular to the occlusal plane. To capture the O-rings following the ideal path of insertion (ideal position), a dental surveyor (B2; Bio-Art Dental Equipment Ltd) was used. The polyurethane matrix was positioned in the horizontal surveyor base, and the attachments were adapted to the mini-implants and captured in pairs with acrylic resin (JET; Clássico Dental Articles) using a test device screwed to the dental surveyor rod (Fig. 3).



Figure 1. Polyurethane resin matrix (20×10×30 mm).

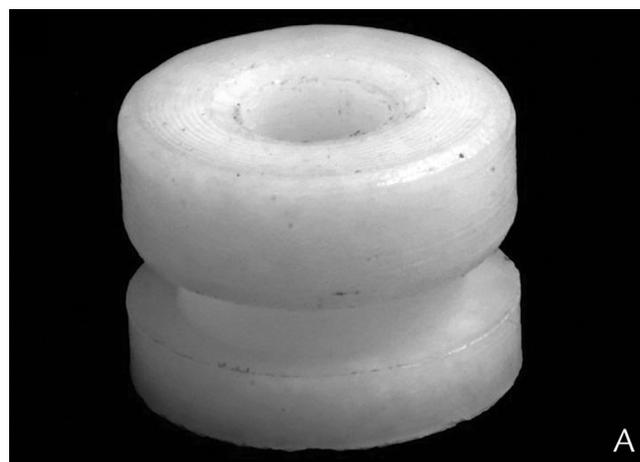
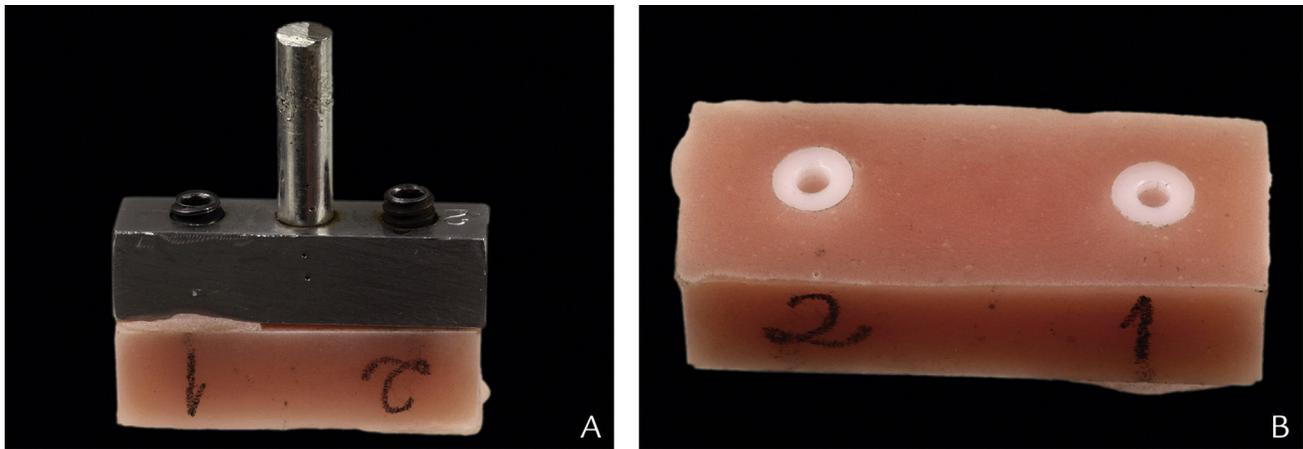


Figure 2. Polymeric attachments. A, Polytetrafluoroethylene (PTFE). B, Polyacetal.

A fatigue resistance testing device<sup>29</sup> in which the insertion/removal axis coincided with the ideal path of insertion was used to simulate the insertion and removal of the overdentures and to assess the retention force of the attachments. To perform the test, the



**Figure 3.** A, Test device for capture. B, Captured attachments.

matrix and resin bases were fixed in the device. A total of 60 attachments were tested during the study (commercial O-ring, polyacetal, and PTFE attachments,  $n=20$  each).

A total of 3625 cycles were performed. Assuming 4 full cycles per day, the test simulated 30 months of overdenture insertion and removal. The test was performed at a rate of 20 cycles per minute and at a constant speed of 35.79 mm/second.<sup>29</sup> The data were analyzed at intervals corresponding to 0, 6, 12, 18, 24, and 30 months of use, and each interval corresponded to the arithmetic mean of 10 consecutive insertion and removal cycles. The force required for each insertion and removal cycle was recorded with the LabVIEW 8.0 software (National Instruments) linked to a load cell in the testing apparatus. The mini-implant and capsule set remained immersed in distilled water at 37°C throughout the test to simulate the temperature conditions found in the oral environment.<sup>30</sup>

An optical stereomicroscope (Discovery V20; Carl Zeiss AG) with  $\times 20$  magnification was used to assess the deformation of the newly developed devices in comparison with the commercial O-ring. Two methods were selected for the quantitative analysis of the deformation. In the first, internal horizontal length (IHL) and external horizontal length (EHL) and internal vertical length (IVL) and external vertical length (EVL) measurements of the attachments were obtained. In the second, internal diameter (ID) and external diameter (ED) measurements were obtained by selecting 3 points (Fig. 4). The measurements were acquired before and after the fatigue resistance test.

After verifying the homogeneity of the data through graphic analysis (residual plotted against predicted values), a repeated measures ANOVA was applied, followed by the post hoc Tukey honestly significant difference test ( $\alpha=.05$ ).

## RESULTS

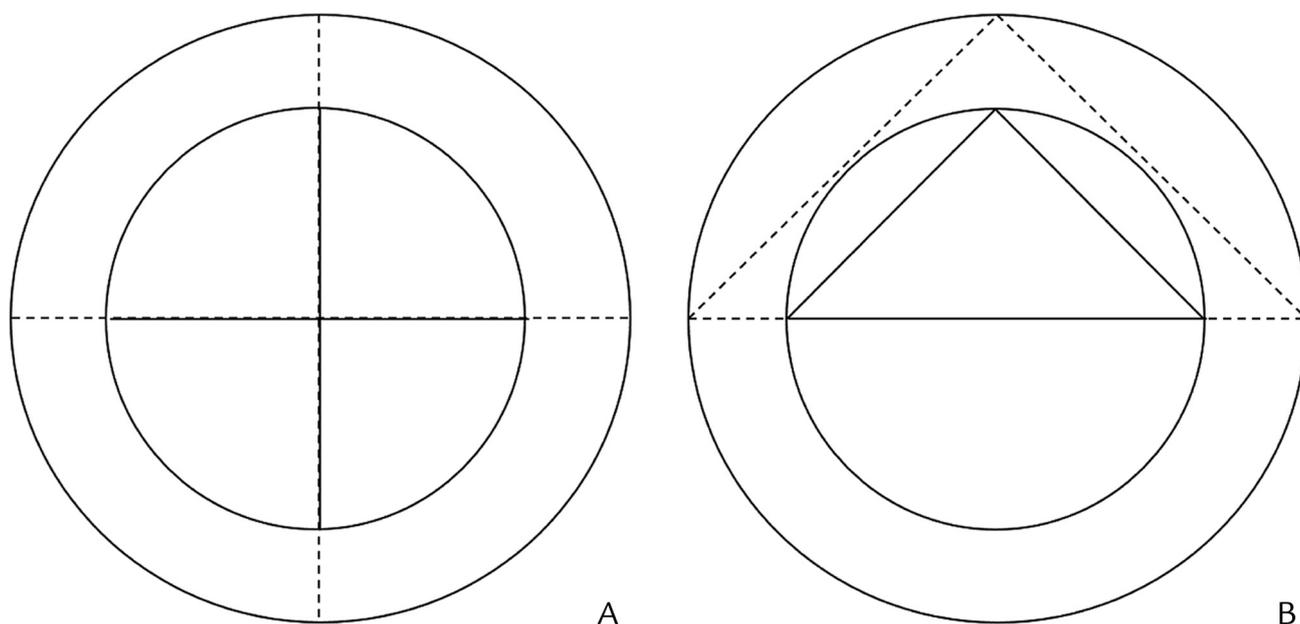
The ANOVA showed that the different attachment materials affected the retention force. A significant difference was observed between the 3 attachment systems: metal, polyacetal, and PTFE ( $P<.001$ ). The polyacetal showed the greatest retention force, followed by the metal and PTFE attachments ( $P<.001$ ). However, no significant change was noted over time ( $P=.071$ ) (Table 1).

The deformation of the different attachment materials was analyzed with an optical stereomicroscope before and after the fatigue resistance test. The results from the horizontal, vertical, internal, and external measurements revealed significant differences among the attachment systems ( $P<.001$ ). The metal attachments had the smallest deformation, followed by the polyacetal and PTFE attachments ( $P<.001$ ) according to the internal horizontal length and internal vertical length measures, but no significant differences were observed between polyacetal and PTFE regarding the EHL ( $P=.813$ ) and EVL ( $P=.793$ ). The 3-point method of measurement had similar results. The metal attachments had the smallest deformation ( $P<.001$ ) based on the ID and ED measures, and no significant differences in the ED were observed between polyacetal and PTFE attachments ( $P=.947$ ) (Table 2).

Changes in the attachment system over time were significant only for polyacetal, with greater deformation observed after the experiment ( $P<.001$ ) (Table 3). The deformation of the mini-implants measured before and after the resistance fatigue test did not show a significant difference for EHL ( $P=.970$ ), EVL ( $P=.941$ ), and ED ( $P=.867$ ).

## DISCUSSION

Synthetic biomaterials, such as PTFE and polyacetal, have significant advantages.<sup>27</sup> The high chemical



**Figure 4.** Quantitative analysis of deformation. A, Measures of horizontal and vertical length, both internal (continuous line) and external (dotted line). B, Measures of internal (continuous line) and external diameters (dotted line).

**Table 1.** Mean retentive forces (N)  $\pm$  standard deviation of each material over time

Time (mo)	Retention Force (N)		
	Metal	Polyacetal	PTFE
0	16.11 $\pm$ 4.17 <sup>a</sup>	18.23 $\pm$ 3.74 <sup>b</sup>	6.63 $\pm$ 1.68 <sup>c</sup>
6	13.80 $\pm$ 2.28 <sup>a</sup>	22.15 $\pm$ 4.84 <sup>b</sup>	5.59 $\pm$ 1.15 <sup>c</sup>
12	13.72 $\pm$ 2.45 <sup>a</sup>	22.85 $\pm$ 4.91 <sup>b</sup>	5.47 $\pm$ 1.14 <sup>c</sup>
18	13.17 $\pm$ 2.73 <sup>a</sup>	23.61 $\pm$ 5.35 <sup>b</sup>	5.48 $\pm$ 1.15 <sup>c</sup>
24	13.22 $\pm$ 2.35 <sup>a</sup>	23.58 $\pm$ 5.86 <sup>b</sup>	5.42 $\pm$ 1.11 <sup>c</sup>
30	13.09 $\pm$ 2.55 <sup>a</sup>	23.79 $\pm$ 6.25 <sup>b</sup>	5.42 $\pm$ 1.21 <sup>c</sup>

PTFE, polytetrafluoroethylene. Same superscript lowercase letters in same column indicate statistical similarity.

resistance of these materials minimizes the degradation from denture-cleaning solutions, and the low cell adhesion reduces microbial surface colonization.<sup>28</sup> Although the use of metal attachments with an O-ring for overdenture retention has been established,<sup>8</sup> the characteristics of synthetic biomaterials justify their use for producing prosthetic components.

Reports on the minimum retention value for mini-implant-retained overdentures are lacking; values<sup>9,11,25</sup> ranging from 3.92 to 9.64 N have been reported. This retention is significantly lower than that of standard implants, which require at least 20 N for acceptable overdenture performance.<sup>23</sup> The polyacetal attachments tested in the present study result in higher retention than the commercial O-rings tested and have a retention value similar to that obtained when using standard implants. Thus, the results support the rejection of the null hypothesis that the different attachments tested would

have no influence on the retention force and deformation components.

The highest retention force ( $P < .001$ ) during the simulation of 30 months of prosthesis use was obtained with the polyacetal attachment (23.79 N), followed by the control O-rings (13.09 N) and the PTFE (5.42 N) attachments. One study using O-rings for mini-implant-retained overdenture attachments reported retention values ranging from 4.49 to 5.90 N,<sup>21</sup> and another study reported a mean retention value of 6.30 N<sup>11</sup>; these values are much lower than those observed for the proposed polyacetal capsule. PTFE, however, showed intermediate values, despite its excellent properties. Given that a mean of 3.92 N suffices for mini-implant retention and a good patient treatment satisfaction index,<sup>11</sup> the attachments developed in this study, especially the polyacetal attachments, showed excellent overdenture retention.

The wear and tear of components of an overdenture attachment system is caused by functional loads, the prosthesis insertion and removal trajectory, implant angulation,<sup>24</sup> and the presence of parafunctional habits<sup>23</sup> and the prosthodontic complication most commonly found (33%) among implant-supported restorations.<sup>4,18,22</sup> It typically occurs in the first 12 months of use, increasing the need for periodic maintenance.<sup>18-20</sup> In this study, O-rings had an 18.7% loss of retention after a simulated 30 months of use, whereas polyacetal had a 30.5% increase and PTFE had an 18.2% reduction. These results were better than those of other studies<sup>18,29</sup> that found a 16.6% loss of retention for O-rings after a

**Table 2.** Mean deformation (mm) ±standard deviation of each material in different methods

Material	Method					
	IHL	EHL	IVL	EVL	ID	ED
Metal	1.30 ±0.05 <sup>a</sup>	3.82 ±0.07 <sup>a</sup>	1.31 ±0.06 <sup>a</sup>	3.83 ±0.09 <sup>a</sup>	1.31 ±0.05 <sup>a</sup>	3.84 ±0.07 <sup>a</sup>
Polyacetal	1.61 ±0.30 <sup>b</sup>	4.47 ±0.17 <sup>b</sup>	1.62 ±0.31 <sup>b</sup>	4.51 ±0.13 <sup>b</sup>	1.63 ±0.32 <sup>b</sup>	4.53 ±0.14 <sup>b</sup>
PTFE	1.75 ±0.05 <sup>c</sup>	4.49 ±0.15 <sup>b</sup>	1.73 ±0.08 <sup>c</sup>	4.45 ±0.30 <sup>b</sup>	1.73 ±0.07 <sup>c</sup>	4.54 ±0.13 <sup>b</sup>

ED, external diameter; EHL, external horizontal length; EVL, external vertical length; ID, internal diameter; IHL, internal horizontal length; IVL, internal vertical length; PTFE, polytetrafluoroethylene. Same superscript lowercase letters in same column indicate statistical similarity.

**Table 3.** Mean deformation (mm) ±standard deviation of each material in different methods and times

Material	Time	Method					
		IHL	EHL	IVL	EVL	ID	ED
Metal	Before	1.29 ±0.03 <sup>a</sup>	3.81 ±0.09 <sup>a</sup>	1.28 ±0.03 <sup>a</sup>	3.81 ±0.10 <sup>a</sup>	1.29 ±0.03 <sup>a</sup>	3.83 ±0.08 <sup>a</sup>
	After	1.32 ±0.05 <sup>a</sup>	3.83 ±0.06 <sup>a</sup>	1.33 ±0.07 <sup>a</sup>	3.85 ±0.07 <sup>a</sup>	1.34 ±0.04 <sup>a</sup>	3.85 ±0.06 <sup>a</sup>
Polyacetal	Before	1.47 ±0.35 <sup>a</sup>	4.46 ±0.15 <sup>a</sup>	1.49 ±0.36 <sup>a</sup>	4.51 ±0.11 <sup>a</sup>	1.48±0.40 <sup>a</sup>	4.52 ±0.10 <sup>a</sup>
	After	1.75 ±0.15 <sup>b</sup>	4.48 ±0.18 <sup>a</sup>	1.76 ±0.17 <sup>b</sup>	4.52 ±0.15 <sup>a</sup>	1.79 ±0.04 <sup>b</sup>	4.54 ±0.17 <sup>a</sup>
PTFE	Before	1.72 ±0.05 <sup>a</sup>	4.46 ±0.16 <sup>a</sup>	1.69 ±0.06 <sup>a</sup>	4.39 ±0.39 <sup>a</sup>	1.70 ±0.06 <sup>a</sup>	4.52 ±0.12 <sup>a</sup>
	After	1.78 ±0.03 <sup>a</sup>	4.51 ±0.15 <sup>a</sup>	1.77 ±0.06 <sup>a</sup>	4.51 ±0.15 <sup>a</sup>	1.76 ±0.06 <sup>a</sup>	4.56 ±0.13 <sup>a</sup>

ED, external diameter; EHL, external horizontal length; EVL, external vertical length; ID, internal diameter; IHL, internal horizontal length; IVL, internal vertical length; PTFE, polytetrafluoroethylene. Similar superscript lowercase letters in same column (before and after) for each material indicate statistical similarity

simulated 6 months of prosthesis use and a 57.1% loss after 24 months.

The 2 analysis methods used showed similar results regarding the measurement of deformation using an optical stereomicroscope. Polyacetal and PTFE had greater IHL, IVL, and ID deformation than the conventional O-rings, and after performing the fatigue test, the greatest deformation was observed in the polyacetal attachments. This result may be related to the increased retention (18.23 to 23.79 N) of this material during the 30-month simulation because the increase in surface roughness or hardening of some polymer components increases rather than decreases the retention force. Another likely reason for the increase in retention is the possible thermal expansion of the material during the experiment, which was performed with distilled water at 37°C to simulate conditions in the oral cavity.<sup>18,30</sup>

The commercial O-ring attachments tested experienced less EHL, EVL, and ED deformation than the polyacetal and PTFE attachments because metal has a higher mechanical resistance than polymers. However, this deformation had no effect on the retention of the new devices, especially in the case of polyacetal, which obtained the highest retention after 30 months. The findings of this study agree with those of others reporting an improvement in overdenture retention provided by mini-implants as an alternative solution to conventional prostheses.<sup>1,10,13</sup>

The limitations of this study are associated with its in vitro characteristic, which makes it difficult to simulate the exact conditions found in the buccal cavity. Thus, long-term follow-up clinical studies are

recommended to confirm the results found in the present in vitro study.

**CONCLUSIONS**

Based on the findings of this in vitro study, the following conclusions were drawn:

1. The polyacetal attachment showed higher retention than the commercial O-ring model tested.
2. Despite the deformation experienced by the material, polyacetal attachment should last for at least 30 months before replacement.

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