



Inclusion of graphene on LDPE properties

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ABSTRACT

The spread of graphene in low-density polyethylene (LDPE) improves LDPE/graphene nanocompounds' thermal/mechanical/electrical characteristics. The images of scanning electron microscopy (SEM) verify full graphene exfoliation at 1000 °C. Inclusion graphene develops crystallinity; increases the local order of lattice and thermal stability of LDPE/graphene nanocompounds. The consistent distributions and further inclusion of graphene caused the great heat breakdown strength, increasing heat breakdown activation energy and a superior melting point (T_m) for LDPE nanocompounds. Percolation occurs with the graphene incorporation of 0.5 wt%. The complex viscosity test showed Newtonian behavior for LDPE at a very low frequency. But, graphene inclusion to LDPE changed the viscosity performance from liquid-like to solid-like which caused a decrease in the melt flow rate (MFR) values for all LDPE/graphene nanocompounds.

1. Introduction

A specific class of materials are identified for enhancing characteristics through polymer nanocompounds and nanotechnology, where nanofillers are displayed in the polymer matrix and result in improved mechanical and physical properties [1,2,3,4]. Nanofillers are prominent additives that enhance the characteristics of polymers and nanocompounds that are distinctly lightweight with outstanding mechanical properties [5]. Nanofillers' huge external surface makes superior contact with polymer chains and improves the complex interface morphology, which is compared with pure polymers [6]. Because of the huge value of the width/height ratio and strong Vander-Waals, intermolecular attraction forces between graphene layers, graphene's natural performance is transformed away by stacking [7,8,9,10,11]. In this method, the agglomeration of graphene makes restricted contact with the structure of polymers and prevents its competent functions from being shown [12]. The huge external surface areas of graphene are useful if graphenes are distributed uniformly in the polymer structure, or else graphene agglomerate and the enormous exterior contacts will be ineffective. It was examined that incorporating typical nanofiller gives specific property, for instance, physical, chemical, electrical and mechanical characteristics to the produced polymer nanofiller nanocompound [13,14,15]. The point of incorporating nanosize fillers with the polymer matrix is due to their enormous internal surface area [16,17,18,19].

Graphene, a two-dimensional nanomaterial with single atomic thickness and a single layer of sp^2 hybridized carbon particles, is used for its wonderful characteristics, such as incredible electrical conductivity, fire extinguisher, exceptional thermal and mechanical characteristics, and so on [20,21,22]. These wonderful characteristics of graphene are accompanied by its simple manufacturing process make graphene a great nanofiller for various materials [23]. However, the thickness of graphene varies from mono to few layers that are a few nanometers; the other sides are in micron, providing a notable percentage of width/height ratios along with an abundant specific external surface area (2620–2960 m^2/g for fully delaminated graphene). Unlike nanoclay filler, graphene provides a lower mass density, a wonderful electrical and thermal conductivity product owing to its sp^2 -hybridized carbon atom connections and the non-existence of scattering-electron [24]. Thus, the applications of graphene polymer nanocompounds in various research centres have shown tremendous benefits. In some cases, graphene works superior to carbon nanotube (CNT) because the inward surface of CNTs is not easily possible for polymers to get in, and therefore makes graphene more appropriate than CNT to expand the basic purposes explicitly in the materials' electrical, thermal, mechanical and microwave properties [12, 23,25,26]. The other aim of using graphene, as opposed to CNT, is its reasonable cost. Graphene is developed through using graphite, an abundant element, and a straightforward and simple process in research centers. But CNTs are actually produced through complex and costly

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methods, such as chemical vapor deposition and laser vaporization; however graphene is produced via mechanical delamination from untreated graphite. Graphene multilayers have different graphene layers in platelet-like graphite nanocrystals [27,28,29]. Since graphene has a huge interaction with the polymer in a polymer/graphene synthesis, at that stage the applied stress transfers from polymer to graphene, which enhances the mechanical characteristics of the nanocompounds [30]. The role of graphene in polymer nanocompounds is considerably feasible compared to other performance fillers which are due to exceptional width/height ratio (600–10000) of graphene [31]. Graphene's two-dimensional arrangement delivers a huge interaction with the polymer arrangement and increases the nanocompound's thermal conductivity [32]. In addition, each graphene layer has some inconsistent characteristics as its molecular structure is not penetrable and it can be implemented as protective shields against electromagnetic waves for small particles comparable to H₂ or noble gasses. Graphene's mechanical characteristics are also remarkable as its great Young module is approximately 1 TPa [33]. Graphene nanocompounds have a wonderful deterrent to oxygen penetration due to very tiny holes available in the surface of graphene. Because of the graphene sponginess and planar structure, graphene blocks O₂ penetration through the development of a tortuous path in polymer-graphene nanocompounds and makes it as a proper replace material for the gas tanks [34]. Graphene nanocompounds have a wonderful barrier to maintain oxygen permeation due to the tiny holes at the graphene interface and LDPE, and graphene-based polymers are consequently being considered proper substitute materials for fuel tanks [35]. It was studied that inclusion of graphene to polymers enhances the nucleation process in the earlier stage of crystallization with decreasing operating active energy.

This analysis is aimed at designing, developing and characterizing a polymer nanocomposite through inserting nanoplatelets of graphene into the LDPE matrix. Once its mechanical characteristics have been improved, LDPE was selected as the network material to use the prepared composite as basic material. In order to evaluate the morphology of nanofillers' composites and sizes, SEM, transmission electron microscopy (TEM), X-ray diffraction (XRD) and Raman spectra (RS) studies were conducted and mechanical and thermal characteristics were evaluated on nanocomposite specimens with other devices. To examine mechanical characteristics, a dynamic mechanical analyzer (DMA) and strength tester were implemented. The huge external surface areas and the greater graphene characteristics have enhanced nanocompounds' thermal stability, heat and electrical conductivity, storage modules, and mechanical properties. With further incorporation of graphene in the LDPE structure, the electrical conductivity, thermal stability and viscosity of graphene nanocompounds are elevated.

As a result, graphene incorporation advances nucleation processes in the main crystallization phases revealed by decreasing operational active energy. The aim of this research is to produce, manufacture and categorize graphenes for incorporation in LDPE structures. LDPE is a low cost, easily reusable, engineered thermoplastics mainly for packing, electrical cables, water, and oxidation resistance which are chosen in place of a polymeric nanocompounds with significant commercial importance [36, 37,38]. Graphene is employed in major researches and considerations specified in the sciences of physics, chemistry, bioscience, and materials [39]. Its absolute characteristics, such as superior electrical conductivity, mechanical elasticity, thermal conductivity, and visual clarity, provide different responsibility and cause it to be notable theoretically [40]. The function of nanofiller in preparation of polymer nanocompounds has been studied extensively [41,42,43,44]. Graphene has an enormous external surface area and the formation of long-range carbon-carbon connectivity for suitable mechanical and electrical characteristics of polymer nanocompounds is achieved even at an amount lower than the CNT nanofiller [45,46,47,48]. This study concentrates on preceding knowledge of graphene-polymer nanocompounds by studying the impact of compounding states on LDPE/graphene nanocompounds' characterization, electrical, thermal conductivity, and mechanical characteristics.

In order to enhance macromolecular science and engineering, this study is focused on analyzing contemporary subjects of nanocompound graphene applications. This work in the field of melt processed graphene-polymer composites investigates the impact of nanocomposite conditions and inclusions of graphene on the electrical, thermal and mechanical characteristics of LDPE/graphene nanocompounds. This research explored the impact of the incorporation of graphene to boost melting temperature (T_m), better tensile strength and greater LDPE/graphene composite storage modulus. High storage modulus and loss modulus of LDPE/graphene nanocompounds demonstrated that graphene improved comprehensive viscoelasticity of LDPE. When graphene incorporation was 0.5 wt%, some characteristics of LDPE/graphene nanocompounds such as tensile strength, storage modulus, loss modulus, and young modulus were considerably enhanced. This specially designed procedure gave the idea of preparing nanocompounds of graphene/thermoplastic.

2. Materials and methods

2.1. Materials

LDPE as LH0075 pellets, a density of 0.921 g cm⁻³, and a melt flow index of 0.89 g/(10 min), is procured by the Bandar Imam Petrochemical Company (Iran). Graphene with Purity upper than 98 wt%, size 2–10 μ m, thickness, 1–3 nm, explicit outer surface territory, 500–700 m²/g, the density of 5–10 mg/ml, dark shading, was purchased from Nano-arrangement and Amorphous Materials Incorporation.

2.2. Materials processing

Using the melt-nanocompounding method, LDPE-graphene nanocompounds are produced using a Haake MinilabII, a mini-lab twin screw mixer, at 190 °C for 10 min at 100 rpm screw speed. Graphene incorporation is set at 0.5, 1.0 and 3.0 wt% in each batch. Samples for categorizations and tests are established using the hot-press casting method for a Carver press at 190 °C. Moreover, a sample of pure LDPE is prepared in the role of a model. The standard and nanospecimens are picked as LDPE and LDPE/graphene. The introduced technique was hot-press-casting which the nanocompound shaped and pressed into a sheet form (square shape) through a hot press and then the samples were chosen for thermal conductivity, loss factor and the remaining waste nanocompounds used for various tests.

2.3. Characterization

SEM (FEI, Quanta 200-E) operating at 25 kV studied the arrangement and shape of samples through the exterior side. Specimens were covered for running SEM with a slight conductive carbon layer. Instead of evaluating nanocompound arrangements, XRD has been implemented by Bruker D-2 phaser, manufactured in Germany, by CuK α curing (π = 1.54 Å) at 30 kV voltage and 10 mA current. The imaging took place from 5°–80° with a ratio of 5°/min. A JEM-200F (JEOL, Japan) TEM at an accelerating voltage of 200 kV was used to determine the arrangement of graphene and LDPE nanocompounds, ultra-fine powders dispersed arranged by ultra-sonication in alcohol and placed via a precise TEM support film. RS was evaluated using 514 nm argon ion lasers on the Lab RAM-HR800 Spectrometer (Horiba, Japan). Thermal gravimetric analysis (TGA) of specimens was conducted using a Q500 system from TA device. The number of carbon-based materials was applied in the air along with 10 °C/min heating level and 25 °C–950 °C heating range. Using DSC-200-F3 (Netzsch Geratebau GmbH, Germany), differential scanning calorimetry (DSC) experiments were performed. In a nitrogen atmosphere, the samples with a median load of 2–4 mg (from -40 °C to 160 °C) were heated by increasing the extent of 10 °C/min. Tensile testing is completed through the Instron 8821S tensiometer using the ISO 527-3 standard procedure, through dumbbells polymeric samples using

techniques of 25 mm scale, 5 mm wide and 2 mm thickness. At ambient temperature, the stress-strain test is used and the elongation rate is 10 mm/min. All mechanical tests are performed using methods for at least four samples and the results are settled on the average quantity. Three samples from each group are arranged and tested likewise to show the repeatability of outcomes. A strain-controlled rotational rheometer (ARES-LS, Rheometric Devices) performs dynamic rheological tests. The MFI analyzer operates to examine thermoplastic materials' melt flow resistance. The MFI apparatus follows the entirely National and International melt flow resistance standards (TMI, USA), as well as BS EN ISO 1133 and ASTM D1238. Temperature is accurately analyzed within the range of 120–450 °C to some extent. Due to the short amplitude shear mode and parallel plate geometry (25 mm diameter), evaluations are grown at 190 °C. Each sample in a 1-mm-thick disk-shaped sample is bent with similar patterns of tensile experiments. Frequency transmits a range (10^2 – 10^{-2}) rad/s used for 3.0% elongation, which affirms the materials' linear viscoelastic behavior. Specimens are assigned 10 min sooner than any frequency sweeping path to keep steady.

3. Analysis

Fig. 1 shows a graphene SEM photograph showing maximum exfoliation at 1000 °C. The layers of graphene have a number of lines on the exterior face. This particular surface arrangement promotes a decrease in accumulation and increases interactions between graphene and LDPE.

Figs. 2, 3, and 4 shows SEM images of pure LDPE and LDPE/graphene 3.0 wt% nanocomposite. The pure LDPE has somewhat rough surfaces (Fig. 2) and reveals the tendency to elongate the upright route. Although the route is compared to the 3.0 wt% nanocomposite elongating trend for LDPE/graphene. The bent lamellar graphene is examined with a highly accurate SEM photograph of LDPE/graphene 3.0 wt% nanocomposite, that is indicated with red indications (Fig. 4).

Fig. 5 shows XRD photos of graphene, pure LDPE and LDPE/graphene nanocomposites using graphene of 0.5, 1.0 and 3.0 wt. XRD analysis was performed to assess the presence of graphene in composites and the results confirmed the semi-crystalline structure of LDPE with a detected peak of about 26° associated with the distance between the different graphene nanoplatelet layers. With the proportion of graphene in the polymer matrix, the amplitude of this peak rises. The extraordinary exterior surface areas show the way graphene layers are agglomerated, and the perception is shown at 26° at a broad weak diffraction peak. The highest point at 26° is associates at (002) of graphite. The two peak points at $2\theta = 20.96^\circ$ and 23.21° are allocated to (110) and (200) lattice planes of LDPE in nanocomposites. By additional graphene

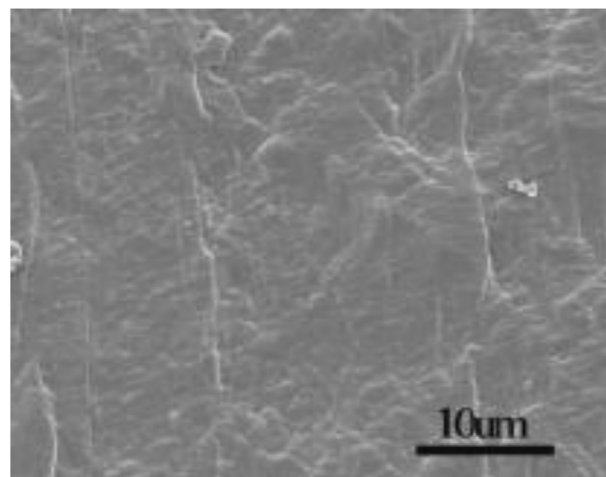


Fig. 2. SEM photograph of pure LDPE.

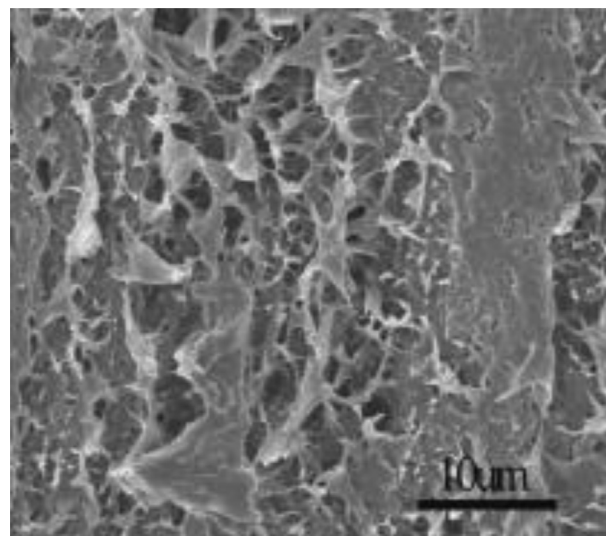


Fig. 3. SEM photographs of surface for LDPE/graphene 3.0 wt%

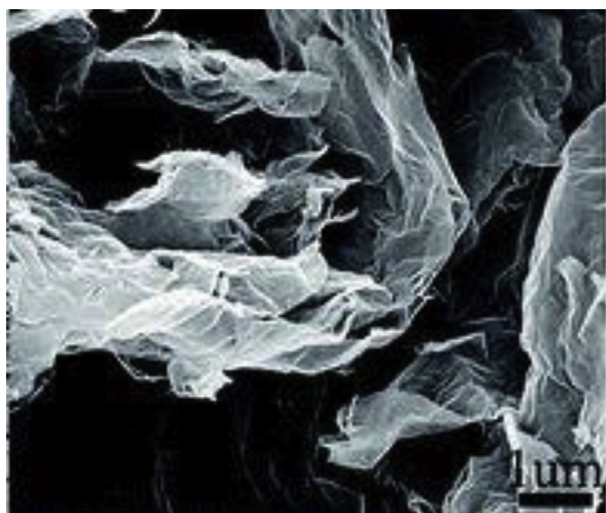


Fig. 1. SEM morphology of graphene.

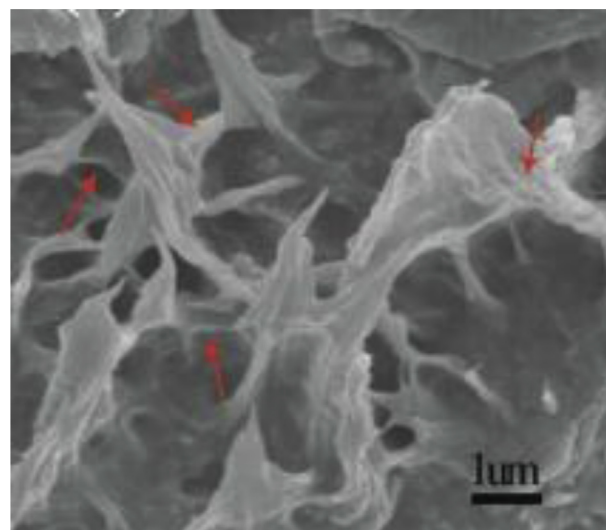


Fig. 4. SEM photographs of surface for LDPE/graphene 3.0 wt%

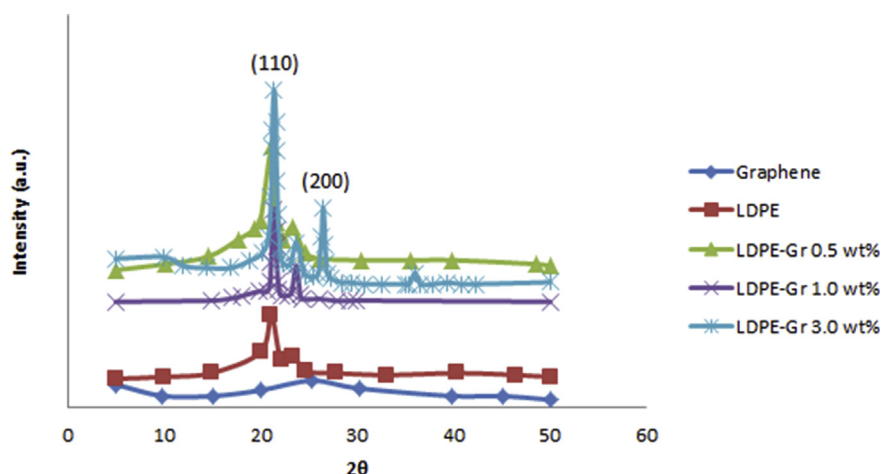


Fig. 5. XRD images of graphene, LDPE and LDPE/graphene nanocompounds.

incorporation, the strength of a diffraction peak makes it sharper, so inclusion graphene increases the LDPE/graphene crystallinity rate. The crystallite size and the crystallinity rate of LDPE/graphenes are increased simultaneously compared to pure LDPE. Both LDPE/graphene 0.5 wt% peak points (1 and 2) are clearer than pure LDPE (Fig. 5). Inclusion of graphene to LDPE simultaneously develops the crystallinity rate and local lattice nanocompound structure.

Fig. 6 displays the graphene TEM photograph. On the surface, the graphene layers were unevenly wrinkled. The appropriate distinctive surface structure displays decrease of accumulation and enhancing interactions between graphene and LDPE.

Fig. 7 shows that these graphene-parts are similarly segregated without accumulation in the LDPE matrix. The clear edges of the lattice in Fig. 7 demonstrate the spread of graphene in the matrix of the LDPE.

Fig. 8 shows the Raman shift of graphene, LDPE, and LDPE/graphene 3.0wt% nanocompound. The flow arrangement at 1355 cm^{-1} and the phase vibration of sp^2 carbon atoms at 1590 cm^{-1} is disclosed by providing a demonstration of RS on graphene. A 2D graphene band disappears due to particular chaos and graphene deficiency. The main property of the chemical bond in polyethylene is C–C reaches out at 1067 cm^{-1} and 1128 cm^{-1} , H–C–H twisting at 1295 cm^{-1} , H–C–H blending at 1441 cm^{-1} and C–H expanding vibration at $2800\text{--}2900\text{ cm}^{-1}$. The connection of polyethylene is revealed through the existence of a C–H group. Raman shifts of LDPE/graphene 3.0 wt% hold the characteristic peak points of graphene and pure LDPE is showing the either LDPE or

graphene combination.

Thermal stability is a property of steadiness that restricts the processing of materials and the use of products. Fig. 9 shows the thermal degradation in the air atmospheric condition of LDPE and LDPE nanocompounds with different weight quantities of nanofillers. The findings indicate that in a single step, the LDPE degradation procedure began at 400°C and was fully completed below 500°C . The weight loss temperature of 5% (T5%) for LDPE occurred at 431°C that associated with thermal deterioration of LDPE commenced primarily by means of thermal breakdowns of C=C pi bonds, with the following progression of radical species, that lessen the molecular weight with de-propagation and inter-transfer and intra-transfer reactions [44]. While the LDPE/graphene nanocompounds thermal breakdown happened through a one-step like LDPE, deterioration began at rising temperatures. With the growing incorporation of nanofiller for nanocompounds, the T5% gradually increases; T5% for LDPE/graphene nanocompounds is improved. Therefore, inclusion of graphene showed superior LDPE thermal stability promotions. These elevations are explained by the graphene's hindrance effect, which is determined in elevating endurance to thermal breakdown and hence inhibiting the spread of LDPE deterioration products in the gas phase [45]. This stability is attributed to enhance interface connections between graphene, LDPE and also adequate spread of graphene in LDPE leading to an increase in thermal breakdown activation energy [46]. Ideal thermal stability is provided by LDPE/graphene nanocompounds. So, the amount of interfacial contact inside the graphene-based nanocompounds provides super outcomes and extensive interactions between

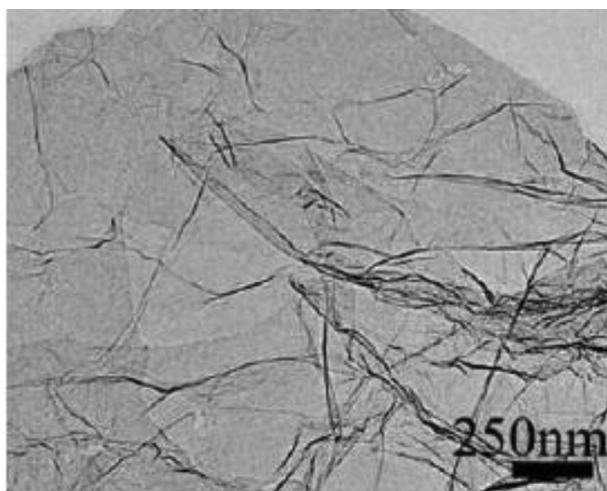


Fig. 6. TEM image of graphene.

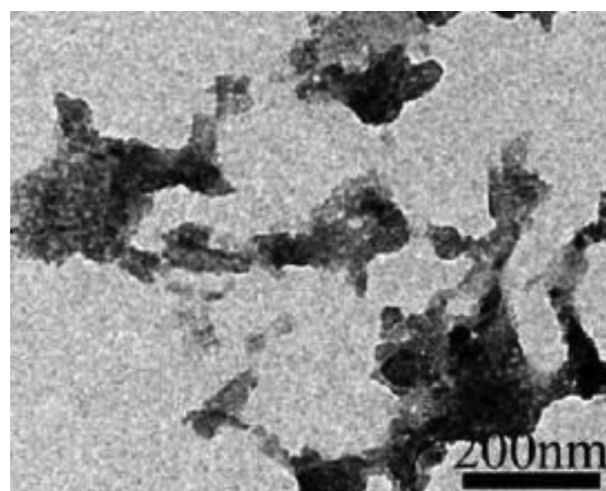


Fig. 7. High-resolution TEM photographs of LDPE/graphene 3.0wt%.

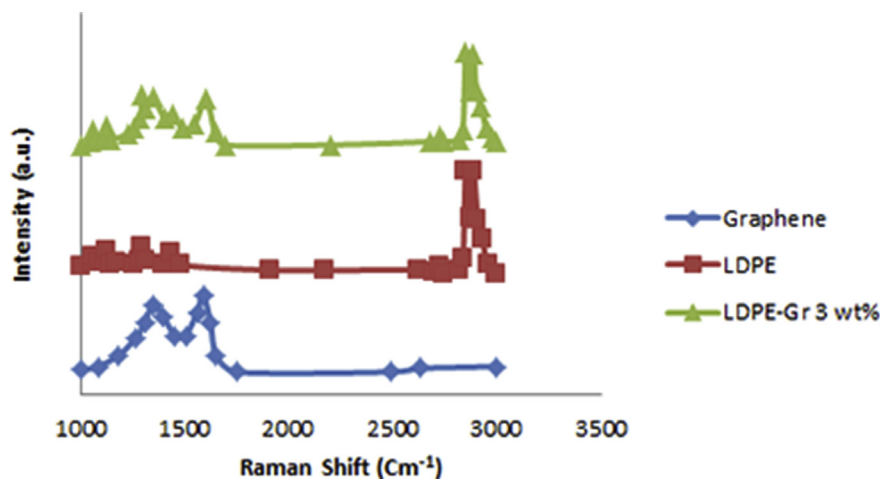


Fig. 8. RS analysis of graphene, LDPE, and LDPE/graphenes 3.0 wt%.

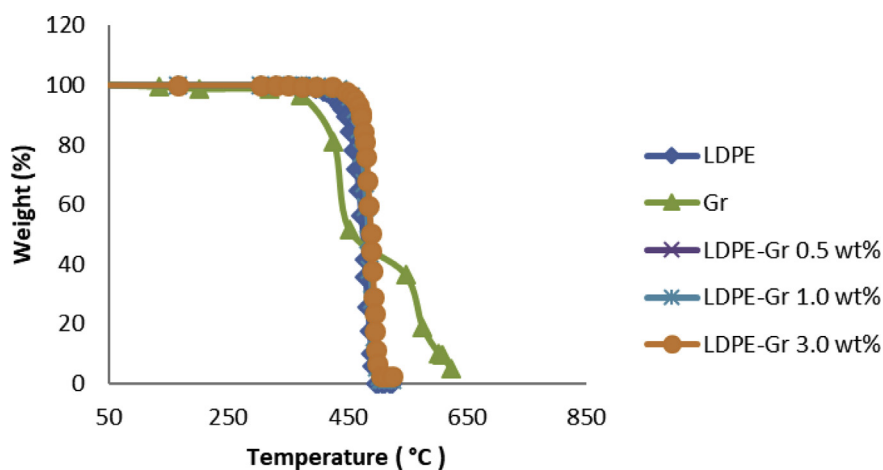


Fig. 9. TGA image of LDPE, graphene and LDPE nanocompounds.

graphene and LDPE.

Fig. 10 demonstrates a DSC test of LDPE, LDPE/graphene and crystallization of LDPE/graphene. The thermograms obtained by the DSC test were evaluated to fully understand the effect of graphene on the LDPE's microscopic structure and the results show that the addition of

nanofillers does not affect the polymer mass percentage crystallinity. In comparison to pure LDPE, T_m of nanocompounds is promoted to 8–9 °C after 0–3.0wt% graphene inclusion. While graphene is spread in LDPE, it folds with the molecular connections and slightly prevents the molecular connection from slipping. The melting procedure, therefore, includes

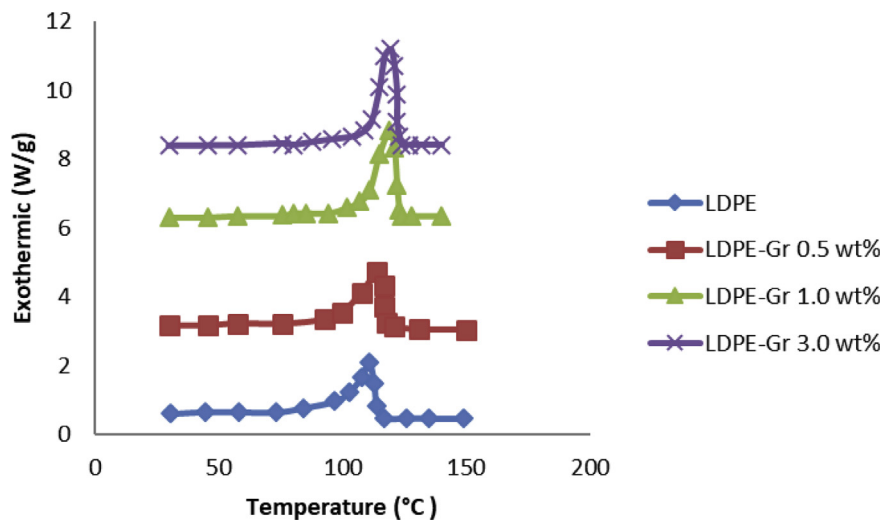


Fig. 10. DSC images of LDPE and LDPE nanocompounds.

additional energy to begin the flow of molecular connections.

Table 1 reports increasing T_m values of LDPE nanocompounds with the additional incorporation of graphene. The heterogeneous nucleation produces higher T_m rates for LDPE/graphene nanocompounds as additional graphene incorporation organizes additional nucleation regions and the level of crystallinity for LDPE/graphene nanocompounds is promoted [1,2,3,4].

Table 1 shows the thermal conductivity of LDPE/graphene nanocompounds. The presence of crystalline in LDPE/graphene nanocompounds improves heat transfer at the boundary of graphene-LDPE in nanocompounds. Thus, thermal conductivity improves with the incorporation of additional graphene into LDPE. LDPE/graphene nanocompounds develop a conductive route that improves the LDPE thermal conductivity [5,6,7,8]. By adding graphene to LDPE nanocompounds, the insufficient thermal and electrical conductivity of pure LDPE is upgraded. Inclusion and homogeneous nano-filler spreading alter the thermal conductivity of LDPE nanocompounds. Table 1 shows that while the quantity of graphene in LDPE increases, thermal conductivity also increases. Graphene nanofiller have high aspect ratios and huge external surface area. Graphene incorporation into LDPE considerably increases the characteristic of heat transfer compared to pure LDPE. Phonons are the fundamental causes in heat conduction of solid materials [9,10,11]. The thermal conductivity of LDPE/graphenes nanocompounds is improved attributable to the conduction mechanism of phonon [12]. Normally, the addition of high conductive additives to LDPE increases nanocompounds' heat conductivity. It was noticed that the thermal conductivity and thermal properties are exposed to the properties of either graphene or LDPE [13,14,15,16,17,18]. Graphene in LDPE are in discrete locations if graphene incorporates in low quantity. The percolation threshold was discovered in this research to be 3.0wt% that the filler aggregates and supply uninterrupted paths to enhance thermal conductivity. The electrical resistivity of LDPE/graphene nanocompounds is available in Table 1. The electrical resistance, reduced quickly in a logarithm test, with the incorporation of 0.5wt% of graphene into LDPE, demonstrating the setup of connected carbons to upgrade electrical conductivity [13,14,15,16,17]. Hence, the percolation phenomenon generates with 0.5wt% addition of graphene to LDPE. This formation of long-range connective carbons is mainly due to the aggregation of graphene throughout the nanoplatelet framework and magnificent structure.

All experimental results in Table 1 showed how T_m values, some typical mechanical features, electrical resistance, and flow resistance of LDPE nanocompounds were promoted by the addition of graphene. As a result of the enormous graphene aspect ratio and the formation of strong contacts at the LDPE-graphene nanocompounds boundary, the mechanical performance of LDPE nanocompounds has significantly been enhanced [18,19,20,21,22,23].

Table 1 shows the LDPE and LDPE-nanocompound mechanical characteristics. For instance, Table 1 demonstrates that incorporating additional graphene into LDPE enhances the characteristics such as tensile stress, tensile module, storage module, loss module, yield stress, elastic module, and young modulus. Table 1 presents the mechanical property improvements of LDPE nanocompounds with the various incorporation of graphene. High storage modulus and loss modulus of LDPE/graphene composites showed that graphene developed comprehensive viscoelasticity of LDPE. The actual various functioning of LDPE/graphene nanocompounds are due to; first, graphene is uniformly dispersed in the LDPE matrix, confirmed by different characterization tests, second, the 2D-structure of graphene geometry control and improve the mechanical bonds at graphene-LDPE interfaces [23,24,25,26]; third, graphene has a massive aspect ratio with a huge surface area with 2D-structure geometry causing the impacts for an appropriately transferring stress among graphene and LDPE [12,27,28,29,30].

Table 1 shows MFR results for all nanocompounds of LDPE and LDPE/graphene nanocompounds. Graphene loading and dynamic viscosity are

disproportionate to the MFR outcomes. MFR values are reduced with the addition of graphenes to LDPE. Since, the addition of graphene in LDPE affects more obstruction to molecular motion and subsequently increases the viscosity of the material [31,32,33,34,35,36].

Fig. 11 shows the tensile strain and tensile stress alterations of LDPE and LDPE/graphene nanocompounds. Fig. 11 shows that with higher graphene incorporation, the resulting yielding points, tensile strengths, and module of nanocompounds are rising. The pure LDPE, meanwhile, exhibited the lowest yielding point, module, and stress tensile values. Thus, graphene incorporation showed the enhancement in tensile strength, yielding points and modulus of LDPE nanocompounds. The variety of the nanocomposite's mechanical properties cannot be attributed to a microscopic change in the polymer structure, but only to the macroscopic reinforcing impact of the nanoscale filler existence.

Fig. 12 shows the LDPE and LDPE/graphene nanocompounds storage modules with temperature changes. Fig. 12 demonstrates the decrease of storage modulus values with growing temperature for all LDPE nanocompounds. Fig. 12 demonstrates that the rate of reduction in storage modules for LDPE nanocompounds with 3.0wt% graphene inclusion is smaller than similar nanocompounds with 0.5 wt% graphene and that the biggest fall in storage modules occurs at each temperature for pure LDPE. Therefore, Fig. 12 indicates that graphene inclusion boosts the inter-molecular interaction of LDPE nanocompounds at higher temperatures.

DMA analyzer examines the dynamic execution of the nanocompounds. DMA tests were conducted at 25 °C for LDPE samples with variable graphene content and different frequencies. The results of the study are achieved in Figs. 13 and 14, which represents the exhibition of storage modulus, loss modulus ($\tan(\delta)$) for pure LDPE and LDPE/graphene. It is recognized that at the same time as frequency content and graphene content rises, the storage module increases either. The performance of storage modulus is legitimized alongside with two dissimilar mechanisms. Primarily, the motion of polymer connections is limited by contact among LDPE and graphene due to its enormous exterior surface area which makes the interfaces tough [37,38,39,40]. Second, the incorporation of graphene in LDPE produces a mechanically resilient LDPE network with a greater storage module which tends to boost the nanocompound module [41]. The storage module efficiency as a frequency variable is shown in Fig. 13. Meanwhile, the outcome of DMA test demonstrates the increasing frequency leads to growing the sample storage module for all the samples.

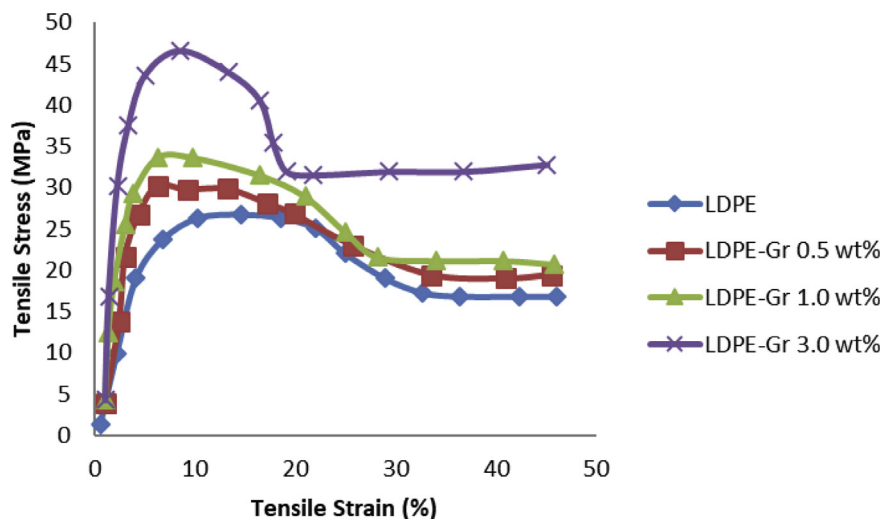
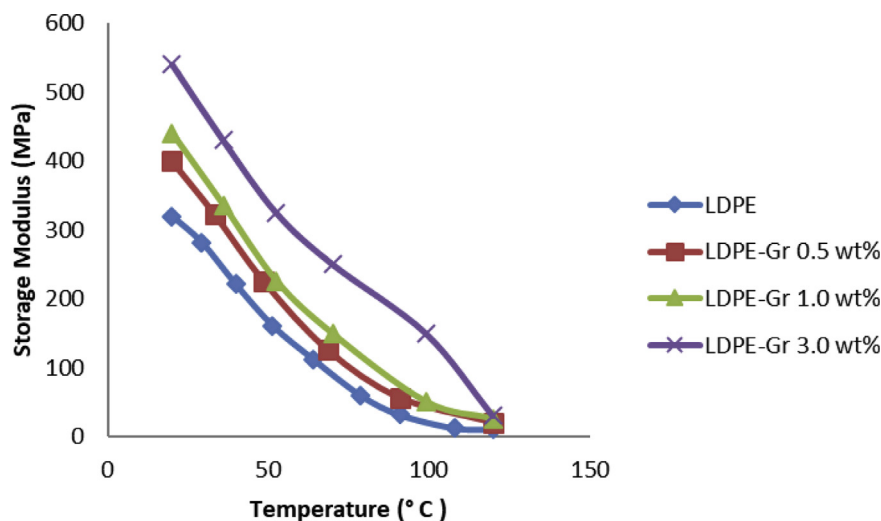
Fig. 15 shows mechanical characteristics enhancements by graphene inclusions (0-3.0wt%) which are seen for tensile strength, yielding stress and elastic modulus tests, however, adding graphene to LDPE reduced the values of elongation at break due to reinforcing impacts of graphene and limited the mobility of polymeric chains.

Fig. 16 and Table 1 demonstrate the development of complicated viscosity by further incorporation of graphene and growing frequencies. The addition of graphene improved the viscosity of the polymer, leading in enhanced processing energy requirements. Figure 16 displays that LDPE followed by a Newtonian pursuing a frequency-free plateau and a shear thinning area at extremely low frequencies, but the upper frequency decreased viscosity values [42,43,44]. Newtonian performance completely vanished with the incorporation of 3.0wt% graphene for the nanocompound samples, showing the parallel linear connections remain unchanged through multiple parameters such as shear thinning performance and viscosity. The viscosity change attributed to the huge surface area, larger aspect ratio, and nanoscale the 2D-flat surface of graphene resulting in an enhanced mechanical interlocking with the polymer chains and enlarged interphase zone at the filler-polymer interface [45]. Wide LDPE restrictions in nanocompounds are therefore well-ordered by incorporating nanofiller. Graphene nanofillers have a superior external surface effect and an elevated graphene aspect ratio that limits LDPE relaxation. Graphene has an enormous internal surface area and a nano-2D-flat surface that makes it resilient to LDPE interface contacts and has an effect on the chain movements of LDPE.

Table 1

LDPE nanocompounds properties.

LDPE/ graphene	T _m (°C)	Thermal Conductivity (W/m.K)	Log (Electrical Resistivity (Ω.Cm)	Tensile Modulus (MPa)	Storage Modulus (KPa)	Loss Modulus at 10 Hz (MPa)	Young Modulus (MPa)	MFR (g/10 min)
Pure LDPE	111.1	0.38	13.5	5.2	0.12	44.86	301.00	0.79
0.5 wt% graphene	114	0.39	11.4	5.32	0.37	45.90	320.00	0.76
1.0 wt% graphene	119	0.40	11.30	5.45	1.23	47.30	329.00	0.75
3.0 wt% graphene	119.5	0.42	11.30	6.5	4.60	52.05	348.00	0.71

**Fig. 11.** Tensile strain and tensile stress of LDPE and LDPE/graphene nanocompounds.**Fig. 12.** Storage modulus of LDPE and LDPE/graphene nanocompounds with temperature alterations.

4. Conclusion

The impacts of graphene have been researched on LDPE's physical, mechanical, electrical and thermal characteristics. Graphene was spread in LDPE to develop nanocompounds of LDPE/graphene. Small graphene adding (0.5wt%) was noted to have a tremendous impact on distinct characteristics, but graphene incorporation above 0.5wt% only creates slight changes on comparable characteristics. As graphene incorporation increased, developments of LDPE's electrical and thermal characteristics

were achieved. The thermal conductivity of LDPE/graphene nanocompounds is developed with further graphene inclusion, uniform graphene dispersion and conductive setup formation in polymer matrix. LDPE's thermal stability has been upgraded by further graphene incorporation. For LDPE nanocompounds with graphene incorporation up to 3.0wt%, elevated tensile strength and high crystallinity were obtained. MFR values reduced by further addition of graphene. The complex viscosity test showed Newtonian behavior of LDPE at a very low frequency, however, graphene inclusion changes viscosity performance from liquid-

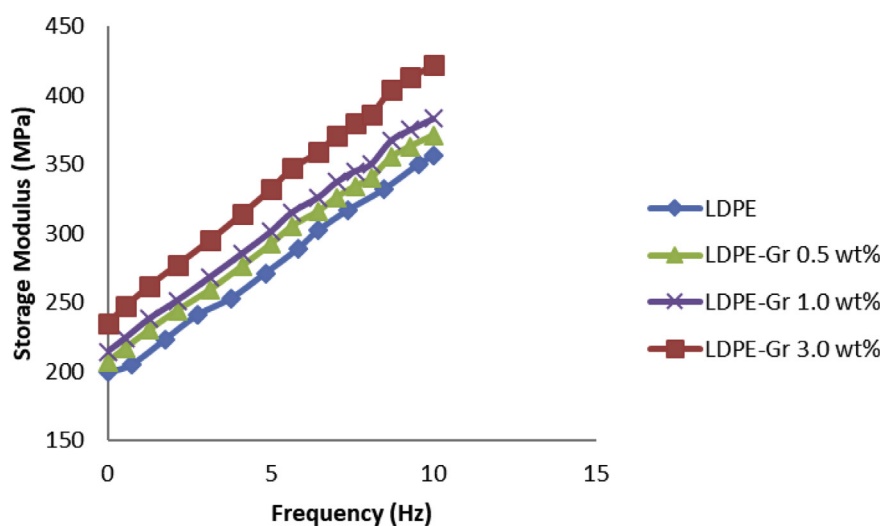


Fig. 13. Storage modulus and frequency alterations of LDPE and LDPE/graphenes with frequency alterations.

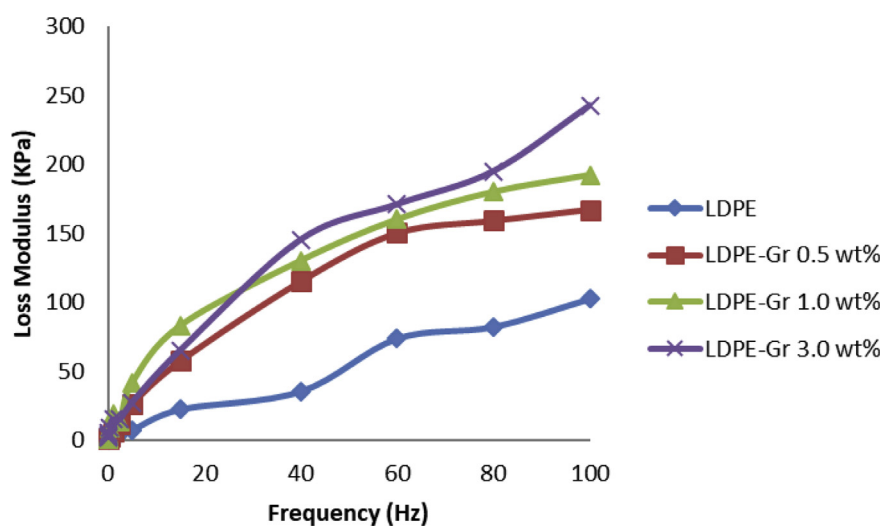


Fig. 14. Frequency alterations and loss modulus on LDPE and LDPE/graphenes.

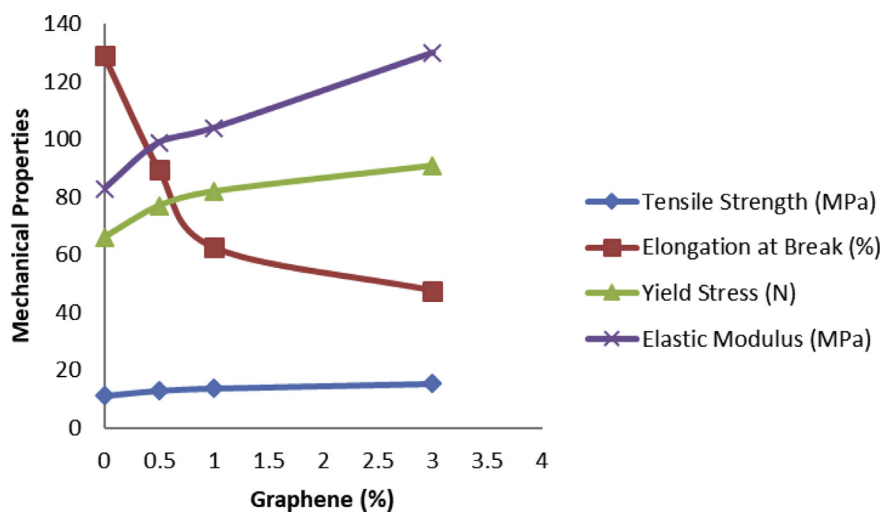


Fig. 15. Typical mechanical properties of LDPE and LDPE/graphenes with graphene inclusions.

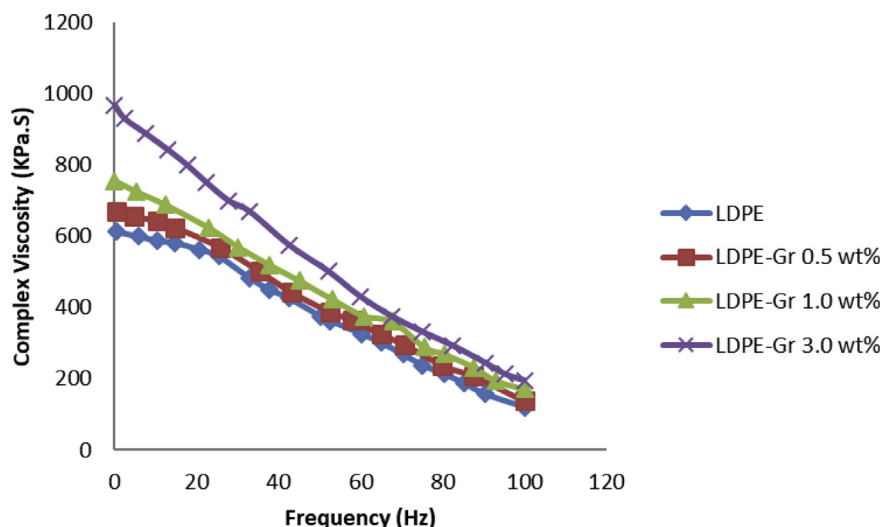


Fig. 16. Complex viscosities of LDPE nanocompounds and frequency alterations.

like to solid-like as a result of the development of interlinked setup arrangements of nanocompounds and hindered the movement of macromolecular polymeric chains which cause MFR values to decrease. The large LDPE/graphene storage module and loss module confirmed that graphene comprehensively enhanced LDPE's viscoelasticity. The graphene loading effects within the nanocompounds were measured by XRD analysis. XRD results promote the semi-crystalline structure of LDPE in accordance with the range between graphene nanosheets films through the recognized peak. The peak amplitude arises with the extra inclusions of graphene within the LDPE. The findings of the thermogram obtained by DSC were investigated with the aim of full recognition and the impact of graphene on the atomic structure of LDPE, the findings show that the inclusion of graphene did not significantly affect the changes in LDPE's crystallinity. DMA results simultaneously express development in the storage and loss module of LDPE nanocompounds. In addition, the composites' stress-strain curve displays a very small plastic region, leading in an almost brittle fracture compared to pristine LDPE owing to the existence of huge agglomerates of graphene. The enhanced outcomes of thermal and electrical conductivity are probably owing to the enhanced graphene dispersion, resulting in more conductive networks being formed. With the addition of graphene to LDPE up to 3.0wt%, the tensile strength improved while the MFR decreased with an enhanced adding of graphene.

Declarations

Author contribution statement

Mazyar Sabet & Hassan Soleimani: Conceived and designed the experiments; Performed the experiments; Analyzed and interpreted the data; Contributed reagents, materials, analysis tools or data; Wrote the paper.

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Additional information

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