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# Masking ability of indirect restorative systems on tooth-colored resin substrates

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## ABSTRACT

**Objective.** To evaluate the masking ability of different indirect restorative systems (IRS) on tooth-colored resin substrates.

**Methods.** A1-shaded specimens from 5 IRS (LDC-IPS e.max<sup>®</sup> CAD; YZW-Zenostar Zr Translucent; PICN-Enamic; YLD-T-IPS e.max<sup>®</sup> ZirCAD+IPS e.max<sup>®</sup> Ceram; CAD-on-Zenostar Zr Translucent+Crystall./Connect+IPS e.max<sup>®</sup> CAD) were fabricated. Specimens (n=5) were cemented with a resin luting agent (Variolink<sup>®</sup> N; shade White) on three different shades (ND3, ND8 and ND9) of a tooth-colored resin substrate (IPS Natural Die Material). Spectral reflectance and color coordinates were measured using a spectroradiometer under standardized lighting conditions (CIE D65 illumination) and optical geometry 0/45°. Color differences ( $\Delta E_{ab}^*$  and  $\Delta E_{00}$ ) from cemented specimens and CIELAB- and CIEDE2000-based translucency parameter ( $TP$  and  $TP_{00}$ ) from non-cemented specimens were calculated. Data was statistically analyzed using one-way ANOVA and Tukey's tests ( $\alpha=0.05$ ).  $\Delta E$  values were also analyzed using perceptibility ( $PT=1.22 \Delta E_{ab}^*$  units;  $0.81 \Delta E_{00}$  units) and acceptability ( $AT=2.66 \Delta E_{ab}^*$  units;  $1.77 \Delta E_{00}$  units) thresholds.

**Results.** The cemented specimens of CAD-on, LDC, YZW and PICN on different substrates (ND3–ND8, ND3–ND9 and ND8–ND9) showed different  $\Delta E_{ab}^*$  and  $\Delta E_{00}$  values ( $p \leq 0.05$ ), which were above AT. YLD-T showed  $\Delta E_{ab}^*$  and  $\Delta E_{00}$  values below AT for all comparisons. Lowest and highest  $TP$  and  $TP_{00}$  values were obtained for YLD-T and PICN, respectively ( $p \leq 0.05$ ).

**Significance.** Resin-cemented YLD-T on different tooth-colored substrates showed less translucency as well as smaller color differences (below acceptability threshold), indicating the best masking ability among evaluated systems.

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## 1. Introduction

Considering dental color appearance, natural-looking restorations require adequate shade matching and blending optical

properties from adjacent natural teeth [1,2]. The final appearance of esthetic indirect restorations is influenced by factors such as composition and microstructure [2,3] optical properties [4] and layering of the ceramic systems [5], surface texture and material thickness [6,7], and color and opacity of luting

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agents [6,7]. In addition, the tooth preparation (substrate) color is major factor influencing on final color and appearance of indirect restorations [1,8].

In clinical situations requiring restoration of non-vital discolored teeth or metal abutment structures, dentists are confronted to choose materials to mask the underlying color producing an adequate esthetic restoration. That is one of the greatest challenges in esthetic dentistry [8,9]. Additionally, the ceramic framework translucency was recognized as a key factor determining the optical characteristics of all-ceramic restorations [10].

There are many CAD–CAM ceramic systems combining strength and esthetics to cover different clinical situations. Lithium disilicate-based glass-ceramic has generated considerable interest for restorative dentistry mostly because of adequate strength (350–450 MPa) [8] and optical properties [4]. Yttria-stabilized tetragonal zirconia polycrystal (Y-TZP) is still the strongest and toughness ceramic ever used in dentistry [8,11] but its limited translucency [12] and the veneer porcelain chipping [11] are major disadvantages for veneered Y-TZP systems [13]. To avoid such problems, monolithic zirconia restorations using highly-translucent Y-TZP were introduced to dentistry as an alternative to porcelain-fused-to-zirconia restorations [14–16]. In addition, in 2011, a new technique was developed (CAD-on) to produce multilayered all-ceramic restorations (zirconia framework and lithium disilicate-based veneer fused together using a glass-ceramic) manufactured using the CAD–CAM technology [17,18]. A polymer-infiltrated ceramic-network (PICN) material with a dominant ceramic-network interconnected to a polymer-based matrix was introduced as an attempt to combine good material properties from polymers and ceramics [19,20].

Different parameters have been used to evaluate the masking ability of restorative materials, such as: contrast ratio (CR) [21,22] and translucency parameter (TP) [9,10,21–25]. In addition, CIELAB color space and its associated CIELAB ( $\Delta E_{ab}^*$ ) and CIEDE2000 ( $\Delta E_{00}$ ) total color difference formulas have been extensively used for color research in dentistry and, as a consequence,  $\Delta E_{ab}^*$  [7,9,10,24,26–29] or  $\Delta E_{00}$  [23,25] have been also used to evaluate the masking ability of restorative materials cemented on colored substrates. Yet, the International Organization for Standardization (ISO/TR 28642:2016) [30] states that color differences should be assessed on the basis of 50:50% acceptability (AT:  $\Delta E_{ab}^* = 2.66$  and  $\Delta E_{00} = 1.77$ ) and 50:50% perceptibility (PT:  $\Delta E_{ab}^* = 1.22$  and  $\Delta E_{00} = 0.81$ ) thresholds [31]. Thus, if the color difference between two specimens is at or below PT, it represents an excellent match; if the difference is between PT and AT, it represents an acceptable match; and if the difference is above AT, it represents an unacceptable match.

As the masking ability of indirect restorative systems (IRS) is critical for acceptable esthetic restorations on discolored substrates, the objective of this study was to evaluate the masking ability of IRS on different tooth-colored resin substrates using CIELAB ( $\Delta E_{ab}^*$ ) and CIEDE2000 ( $\Delta E_{00}$ ) metrics for color differences and the translucency parameters (CIELAB-based TP and CIEDE2000-based  $TP_{00}$ ) for measuring the translucency of non-cemented IRS specimens. The hypotheses tested were that (1) color differences from same IRS cemented on different color of substrate are not accept-

able (above AT), and (2) translucency varies with structural characteristics.

## 2. Material and methods

This *in-vitro* study used five indirect restorative systems (Table 1) being three monolithic structures (LDC, YZW and PICN), one bilayer structure (YLD-T) and one trilayer structure (CAD-on).

### 2.1. Specimens preparation

Plate-shaped specimens ( $n = 20$ ; 1.5 mm thick; and shade A1) were fabricated from pre-sintered CAD–CAM ceramic blocks (IPS e.max<sup>®</sup> CAD, IPS e.max<sup>®</sup> ZirCAD and VITA Enamic<sup>®</sup>) and disc (Zenostar Zr Translucent) using a water-cooled precision cutting machine (Minitom, Struers Inc., Ballerup, Denmark) and diamond disc. Ceramic specimens were polished (Struers Abramin, Copenhagen, Denmark) using a sequence grit of silicon carbide abraded papers (#600, 800, 1200) under constant water irrigation.

For the CAD-on specimens, Zenostar Zr Translucent plates (thickness: 0.7 mm) were sintered (Zirkonofen 600/V2 furnace, ZirkonZahn, Gais, South Tyrol, Italy) according to the manufacturer's instructions. These zirconia plates were glass fused (IPS e.max CAD Crystall./Connect) to 0.7 mm thick plates of IPS e.max CAD HT. For this, the fusion glass capsule containing powder and liquid was vibrated (Ivomix, Ivoclar Vivadent, Schann, Liechtenstein) for 10 s, opened, and the material was applied to the surface of the IPS e.max<sup>®</sup> CAD HT plate that was immediately positioned onto the zirconia plate. The three-layer structure was placed under a load of 750 g and the excess glass was removed with a brush. Glass fusion and glass-ceramic (IPS e.max<sup>®</sup> CAD HT) crystallization were performed simultaneously using a Programat EP5000 furnace (Ivoclar Vivadent, Schann, Liechtenstein) following manufacturer's instructions [17,18].

The bilayer ceramic structure (YLD-T), simulating a conventional ceramic restoration, was fabricated using a plate (thickness: 0.7 mm) of IPS e.max<sup>®</sup> ZirCAD veneered by a layer (thickness: 0.8 mm) of IPS e.max Ceram. The zirconia plate was fabricated as described for CAD-on. The IPS e.max Ceram layer was obtained by the traditional layering technique (powder/liquid). Before application of the ceramic veneer, a thin layer of IPS e.max ZirLiner (Ivoclar Vivadent, Schann, Liechtenstein) was applied onto the zirconia plate and sintered using a Programat EP5000 furnace, according to the manufacturer's instructions. Treated zirconia plate was placed in a silicon matrix (Zetaplus, Zhermack SpA, Badia Polesine, Italy) for ceramic application. IPS e.max Ceram powder and liquid were mixed and applied with a brush onto the treated zirconia surface followed by sonic vibration. Excess ceramic liquid was removed using absorbent paper. The structure was carefully removed from the matrix and placed into the furnace for sintering, following manufacturer's instructions. YLD-T specimens were polished using a sequence grit of silicon carbide abraded papers (#600, 800, 1200) under constant water irrigation.

**Table 1 – Description of materials used in the study.**

Groups	Materials <sup>a</sup>	Thickness	Composition	Indications
LDC	IPS e.max <sup>®</sup> CAD LT	1.5 mm	Lithium disilicate-based glass-ceramics	Monolithic structure
YZW	Zenostar Zr Translucent	1.5 mm	Yttria tetragonal zirconia polycrystal	Monolithic structure
PICN	VITA Enamic <sup>®</sup> HT	1.5 mm	Polymeric-infiltrated ceramic-network	Monolithic structure
YLD-T	IPS e.max <sup>®</sup> ZirCAD	0.7 mm	Yttria tetragonal zirconia polycrystal	Framework ceramic
	IPS e.max <sup>®</sup> Ceram	0.8 mm	Feldspathic ceramic	Veneering ceramic
CAD-on	Zenostar Zr Translucent	0.7 mm	Yttria tetragonal zirconia polycrystal	Framework ceramic
	IPS e.max CAD Crystall./Connect	0.1 mm	Glass-ceramic	Fusion glass
	IPS e.max <sup>®</sup> CAD HT	0.7 mm	Lithium disilicate-based glass-ceramics	Veneering ceramic

All information was provided by manufacturers.  
<sup>a</sup> Except for VITA Enamic (Vita Zahnfabrik, Bad Säckingen, Germany), all materials are from Ivoclar Vivadent (Schann, Liechtenstein).

Handling, preparation, shrinkage percentage calculation (before cutting) and heat treatments (sintering or crystallization) of each ceramic system was performed by the same trained operator following manufacturers' recommendations. Final thickness of specimens was verified with a digital caliper (Digimatic caliper, Mitutoyo Corp., Tokyo, Japan).

## 2.2. Substrate preparation

A light-activated resin-based composite material (IPS Natural Die Material, Ivoclar Vivadent, Schann, Liechtenstein) was used as substrate to simulate tooth-colored preparations. Three different shades (ND3, ND8 and ND9) of this material were used for each IRS (n = 15; and 2.5 mm thick) because of the following reasons:

ND3 — imitates standard dentin (control shade);

ND8 — imitates severely discolored/non-vital tooth preparation; and

ND9 — imitates metallic structures.

A Teflon matrix (14 mm × 14 mm × 2.5 mm) was used to fabricate the substrate plates. The material was packed into the matrix and covered by a mylar strip and a glass slide (thickness: 1 mm). Material was light activated through the glass slide using a curing unit (Radii-cal, SDI, Bayswater, Victoria, Australia; 1200 mW/cm<sup>2</sup>) for 40 s. Plate was removed from matrix and light activated for 40 s from the bottom side.

## 2.3. Cementation procedure

Bonding surfaces of LDC and PICN specimens were etched with 10% hydrofluoric acid (HF — Condac porcelana, FGM, Joinville, SC, Brazil) for 20 s (LDC) and 30 s (PICN). Bonding surfaces of YZW, YLD-T and CAD-on specimens were sand-blasted (Basic classic, Renfert, Ribeirão Preto, Brazil) using aluminum oxide particles (Cobra 25 μm, Renfert, Ribeirão Preto, Brazil) for 20 s with 2 bar pressure. The tip of sand-blasting unit was placed perpendicular and 10 mm far from specimens. Specimens were sonically cleaned (Vitasonic II, Vita Zahnfabrik, Bad Säckingen, Germany) in distilled water for 5 min and air-dried. A thin layer of adhesive (Tetric N-Bond<sup>®</sup>, Ivoclar Vivadent, Schann, Liechtenstein) was applied on the bonding surface of substrates and specimens. Components from the dual-cured cement (White shade; Variolink<sup>®</sup> N, Ivoclar Vivadent, Schann, Liechtenstein) were mixed and

subsequently applied on the treated surface of specimens, which were placed onto the substrates. A load (750 g) was applied on the structures and cement excess was removed with a microbrush (FGM, Joinville, SC, Brazil). Cement was light activated using a curing unit (Radii-cal, SDI, Bayswater, Victoria, Australia; 1200 mW/cm<sup>2</sup>) for 40 s from each side [18].

## 2.4. Reflectance and color measurements

The relative spectral reflectance (between 380–780 nm at 2 nm interval) was measured against white and black backgrounds for each specimen of IRS and against white background for each specimen of IRS cemented on different substrates. This procedure was performed using a non-contact spectroradiometer (SpectraScan PR-670, Photo Research, Chatsworth CA, USA), a fiber-coupled Xe-Arc light source (Oriol Research, Newport Corporation, USA) and a Spectrally Calibrated Reflectance Standard (SRS-3, PhotoResearch, USA). CIELAB coordinates from white and black ceramic tile backgrounds were L\* = 94.70, a\* = 0.06 and b\* = 3.85; and L\* = 22.74, a\* = -0.38 and b\* = -1.67, respectively. Spectral reflectance values were converted into CIE L\*a\*b\* color coordinates using the CIE 2° Standard Observer and the CIE D65 Standard Illuminant. The illuminating/measuring geometry corresponded to CIE 45°/0° [32]. Three short-term repeated measurements without replacement were performed for each sample and the results were averaged.

CIELAB color coordinates against white background were used to evaluate color from all IRS.

## 2.5. Color differences

Color differences ( $\Delta E$ ) values between specimens of the same IRS (n = 15) cemented on different substrates (ND3: L\* = 71.70 ± 0.58, a\* = 2.13 ± 0.16, b\* = 27.86 ± 0.65; ND8: L\* = 61.16 ± 0.83, a\* = 5.68 ± 0.19, b\* = 23.37 ± 0.66; and ND9: L\* = 47.69 ± 1.30, a\* = 1.16 ± 0.11, b\* = 11.35 ± 0.48) were calculated using CIELAB color difference metric ( $\Delta E_{ab}^*$ ) [32]:

$$\Delta E_{ab}^* = \sqrt{(\Delta L^*)^2 + (\Delta a^*)^2 + (\Delta b^*)^2} \quad (1)$$

where  $\Delta L^*$ ,  $\Delta a^*$  and  $\Delta b^*$  are the respectively axes differences for a pair of samples; and CIEDE2000 color difference metric ( $\Delta E_{00}$ ), according to following equation [32,33]:

$$\Delta E_{00} = \sqrt{\left(\frac{\Delta L'}{K_L S_L}\right)^2 + \left(\frac{\Delta C'}{K_C S_C}\right)^2 + \left(\frac{\Delta H'}{K_H S_H}\right)^2 + R_T \left(\frac{\Delta C'}{K_C S_C}\right) \left(\frac{\Delta H'}{K_H S_H}\right)} \quad (2)$$

where  $\Delta L'$ ,  $\Delta C'$ , and  $\Delta H'$  are the differences in coordinates (lightness, chroma, and hue, respectively) for a pair of samples in CIEDE2000.  $R_T$  is the so-called rotation function that accounts for the interaction between chroma and hue differences in the blue region.  $S_L$ ,  $S_C$ ,  $S_H$  are the weighting functions that adjust the total color difference for variation in the location of the color difference pair in  $L'$ ,  $a'$ ,  $b'$  coordinates. Finally, the parametric factors ( $K_L$ ,  $K_C$ ,  $K_H$ ), are correction terms for experimental conditions [32,33]. In the present study, parametric factors of the CIEDE2000 color difference formula were all set to 1 ( $K_L = 1$ ,  $K_C = 1$ ,  $K_H = 1$ ). Discontinuities due to mean hue computation and hue-difference computation were considered to calculate the CIEDE2000 color difference metric [34].

Color differences were analyzed through comparisons with 50:50% perceptibility ( $PT = 1.22 \Delta E_{ab}^*$  units and  $0.81 \Delta E_{00}$  units) and 50:50% acceptability ( $AT = 2.66 \Delta E_{ab}^*$  units and  $1.77 \Delta E_{00}$  units) thresholds, as determined for dental ceramics using TSK fuzzy approximation [31].

## 2.6. Translucency parameter

Translucency parameter (TP) values were determined for all specimens from IRS (n = 5), according to the following CIELAB-based equation [35]:

$$TP = \sqrt{(L_B^* - L_W^*)^2 + (a_B^* - a_W^*)^2 + (b_B^* - b_W^*)^2} \quad (3)$$

where the subscripts B and W refer to color coordinates over black and white backgrounds, respectively. The greater the TP value, the higher the translucency of the specimen.

In addition, the TP was also calculated using CIEDE2000 color difference metric [6,36]:

$$TP_{00} =$$

$$\sqrt{\left(\frac{L'_B - L'_W}{K_L S_L}\right)^2 + \left(\frac{C'_B - C'_W}{K_C S_C}\right)^2 + \left(\frac{H'_B - H'_W}{K_H S_H}\right)^2 + R_T \left(\frac{C'_B - C'_W}{K_C S_C}\right) \left(\frac{H'_B - H'_W}{K_H S_H}\right)} \quad (4)$$

where the subscripts B and W refer to lightness ( $L'$ ), chroma ( $C'$ ) and hue ( $H'$ ) of the specimens over the black and the white backgrounds, respectively. All the other parameters are the same as Eq. (2).

## 2.7. Statistical analysis

Translucency parameter values (TP and  $TP_{00}$ ) for non-cemented specimens from different IRS, and color difference values ( $\Delta E_{ab}^*$  and  $\Delta E_{00}$ ) between the specimens from same IRS cemented on different substrates were statistically analyzed using one-way analysis of variance (one-way ANOVA) and Tukey's multiple comparison tests ( $\alpha = 0.05$ ). The statistical analyses were performed using a standard statistical software package (SPSS 16.0, Chicago, USA).

## 3. Results

CIELAB color coordinates of IRS are shown in Fig. 1. Fig. 2(a and b) show mean and standard deviation values of translucency parameter (TP and  $TP_{00}$ ) for different indirect restorative systems. The behavior of all systems was similar for both translucency parameters. PICN and YLD-T showed, respectively, the greatest and the lowest TP values ( $p \leq 0.05$ ). In addition, LDC and CAD-on showed similar TP values ( $p > 0.05$ ) (Fig. 2(a and b)).

Table 2 shows mean and standard deviation values of color differences ( $\Delta E_{ab}^*$  and  $\Delta E_{00}$ ) between specimens of the same IRS cemented on different substrates (ND3–ND8, ND3–ND9 and ND8–ND9). The behavior of all systems was similar for both color difference metrics. Groups LDC, YZW, PICN and CAD-on cemented on different substrates (ND3–ND8, ND3–ND9 and ND8–ND9) showed different  $\Delta E_{00}$  values ( $p \leq 0.05$ ) for all comparisons. In addition, all these values were above AT (Table 2 and Fig. 3(a and b)). The lowest and the greatest  $\Delta E$  values were registered for ND3–ND8 and ND3–ND9,

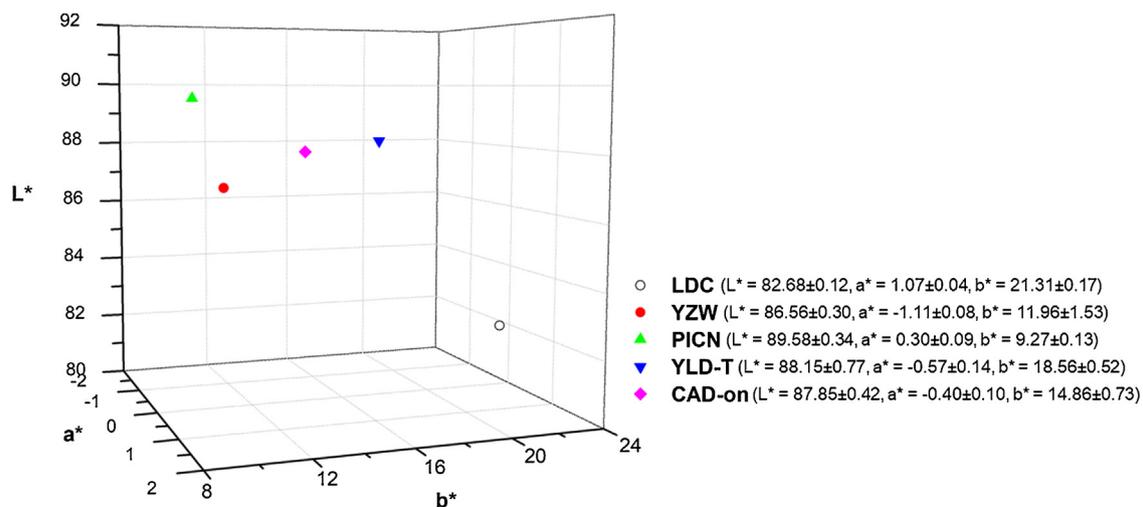
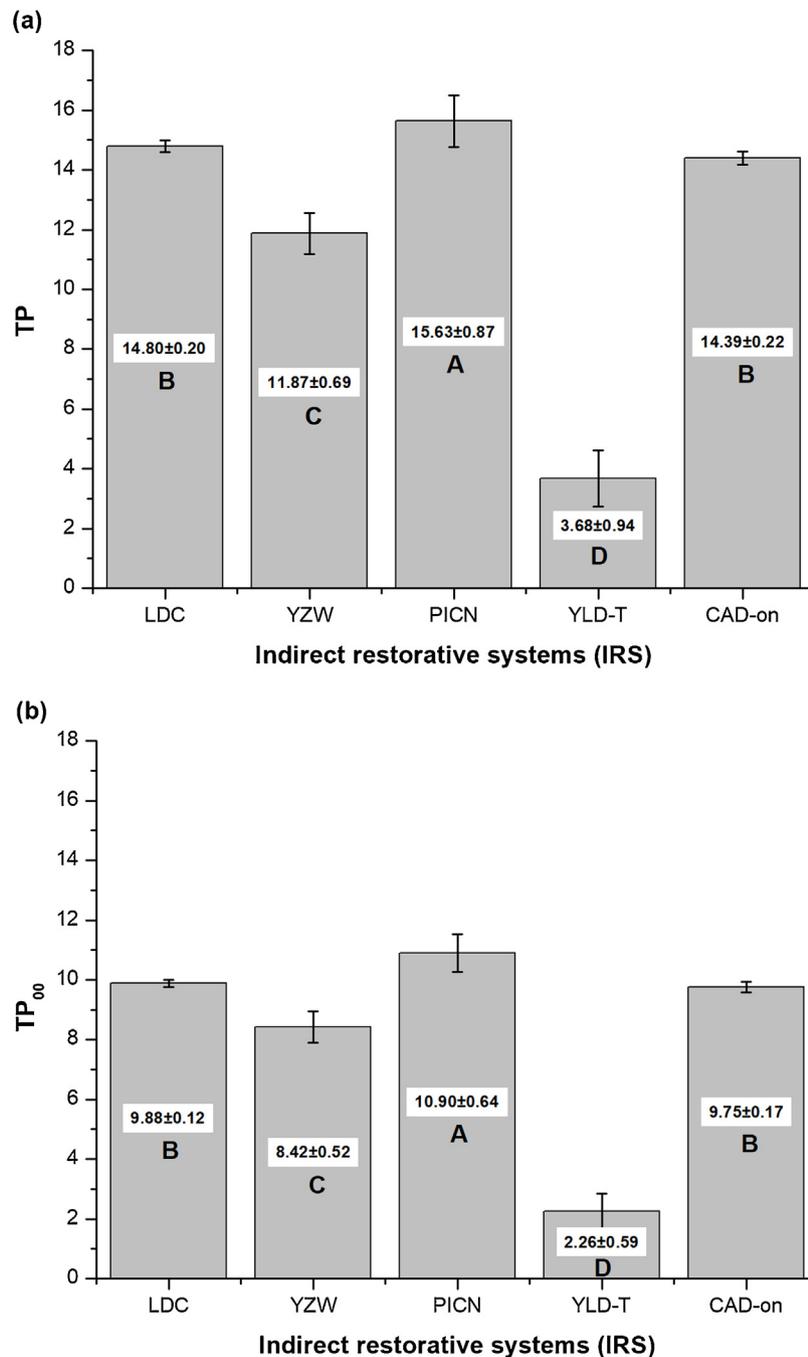


Fig. 1 – Distribution of mean values for the CIELAB color coordinates of each indirect restorative system (IRS), indicated in the figure legend.



**Fig. 2 – Mean and standard deviation values of (a) CIELAB-based translucency parameter (TP) and (b) CIEDE2000-based translucency parameter (TP<sub>00</sub>) for different indirect restorative systems. Different capital letters show statistical differences for mean values of TP or TP<sub>00</sub> (one-way ANOVA and Tukey's tests;  $p \leq 0.05$ ).**

respectively ( $p \leq 0.05$ ) (Table 2). YLD-T showed  $\Delta E_{ab}^*$  and  $\Delta E_{00}$  values below AT for all comparisons (ND3–ND8, ND3–ND9 and ND8–ND9) with some of them not statistically different ( $p > 0.05$ ) (Table 2 and Fig. 3(a and b)).

#### 4. Discussion

The present study was designed to evaluate the masking ability of indirect restorative systems manufactured by CAD–CAM

technology, except for the veneer layer of YLD-T structure. Therefore, monolithic (LDC — lithium disilicate-based glass-ceramics, YZW — zirconia, and PICN — polymer-infiltrated ceramic-network), bilayer (YLD-T — zirconia framework veneered with feldspathic ceramic) and trilayer (CAD-on — zirconia framework and lithium disilicate-based veneer fused with a glass-ceramic) restorative systems were cemented to tooth-colored resin-based composite substrates. The study design was an attempt to mimic clinical challenges of preparations with different shades that need to be masked by an

**Table 2 – Mean and standard deviation values of color differences ( $\Delta E_{ab}^*$  and  $\Delta E_{00}$ ) between specimens from the same indirect restorative systems cemented on different tooth-colored substrates (ND3, ND8 and ND9).**

Substrates	Color differences	Indirect restorative systems				
		LDC	YZW	PIGN	YLD-T	CAD-on
ND3–ND8	$\Delta E_{ab}^*$	4.21 ± 0.30C	4.16 ± 0.74C	5.16 ± 0.49C	1.75 ± 1.18AB <sup>a</sup>	4.61 ± 0.36C
	$\Delta E_{00}$	2.74 ± 0.18c	3.02 ± 0.54c	3.86 ± 0.32c	1.12 ± 0.61b <sup>a</sup>	3.18 ± 0.25c
ND3–ND9	$\Delta E_{ab}^*$	9.74 ± 0.48A	8.73 ± 0.51A	11.51 ± 0.29A	2.42 ± 1.32A <sup>a</sup>	9.93 ± 1.11A
	$\Delta E_{00}$	7.20 ± 0.41a	6.91 ± 0.33a	8.68 ± 0.20a	1.70 ± 0.64a <sup>a</sup>	7.30 ± 0.79a
ND8–ND9	$\Delta E_{ab}^*$	5.80 ± 0.40B	5.22 ± 0.74B	6.77 ± 0.37B	1.47 ± 0.65B <sup>a</sup>	5.94 ± 0.99B
	$\Delta E_{00}$	5.00 ± 0.36b	4.66 ± 0.36b	5.74 ± 0.26b	1.04 ± 0.35b <sup>a</sup>	4.94 ± 0.63b

Statistical groupings resulted from one-way ANOVA and Tukey's tests ( $p \leq 0.05$ ).

Different capital letters show statistical differences for mean  $\Delta E_{ab}^*$  values between the same IRS cemented on different substrates (column) ( $p \leq 0.05$ ).

Different lowercase letters show statistical differences for mean  $\Delta E_{00}$  values between the same IRS cemented on different substrates (column) ( $p \leq 0.05$ ).

<sup>a</sup> Mean values of  $\Delta E$  below acceptability thresholds ( $AT = 2.66 \Delta E_{ab}^*$  units and  $1.77 \Delta E_{00}$  units) (Paravina et al. [31]).

indirect restoration. A previous study [26] used same substrate material to evaluate the influence of different shades of the substrate on the final color of glass-ceramic structures, but used try-in pastes as luting agents.

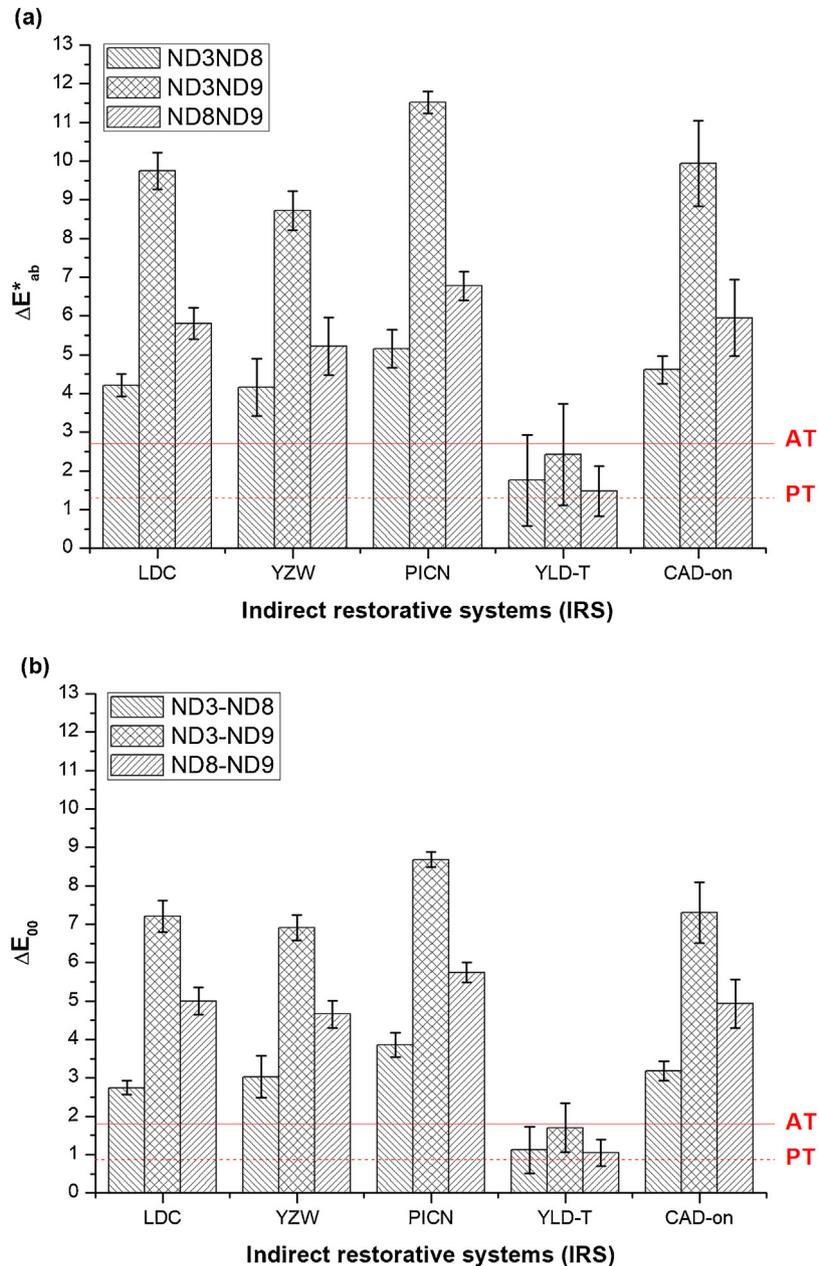
In the present study, color measurements were done using a spectroradiometer. The great advantage of this device is the ability to provide non-contact color measurements, which is obtained under similar viewing conditions as human visual assessments (perceived color) [37]. Most studies on masking ability of different dental materials have used dental spectrophotometers for color measurements [23,26–28]. However, inherent features of human teeth (curved, sometimes narrow, surfaces) challenge these contact-type color measuring devices, which may provide inadequate color readings mostly because of a considerable fraction of light that hits the tooth surface is lost [37,38]. A recent study [39] comparing tooth color measurements obtained by using two devices (a spectroradiometer and a dental spectrophotometer) showed that the combination of a spectroradiometer and CIEDE2000 color difference most closely represents the visual perception of color.

Previous reports have used contrast ratio (CR) [21,22] and TP [9,10,21–25] to evaluate the masking ability of non-cemented specimens and color differences using CIELAB ( $\Delta E_{ab}^*$ ) [7,9,10,24,26–29] or CIEDE2000 ( $\Delta E_{00}$ ) metrics [23,25] for specimens cemented on colored substrates. According to the ISO standard [30], the masking potential of dental materials should be evaluated using TP (color difference against white and black backgrounds). Whenever 1 mm-thick composite or 0.3 mm-thick ceramic shows a TP value below PT ( $\Delta E_{ab}^* = 1.2$ ) it represents an excellent masking potential; a TP value between PT ( $\Delta E_{ab}^* = 1.2$ ) and AT ( $\Delta E_{ab}^* = 2.7$ ) represents an acceptable masking potential; and a TP value above AT ( $\Delta E_{ab}^* = 2.7$ ) represents an unacceptable masking potential [30]. Nevertheless, this standard has some limitations. Materials have to be placed on ideal black and white backgrounds to obtain TP values. These “colors” are opposing extremes and the color difference obtained could be greater than usually involved in dental treatments, such as: vital tooth and non-vital discolored tooth preparations, or vital tooth preparation and a metallic structure (metal post and core or implant abutment), or between a non-vital discolored tooth preparation

and a metallic structure. Therefore, the present study showed that TP and TP<sub>00</sub> values of non-cemented specimens from the evaluated IRS (Fig. 2) were greater than  $\Delta E_{ab}^*$  and  $\Delta E_{00}$  values of same specimens cemented on different substrates (ND3–ND8, ND3–ND9, and ND8–ND9) (Fig. 3), regardless of the parameters used (color difference metrics or translucency parameters), which showed similar behavior (Figs. 2 and 3). In addition, TP values ( $TP = 3.68$ – $15.63$ ; and  $TP_{00} = 2.26$ – $10.90$ ) (Fig. 2) were above AT ( $2.66 \Delta E_{ab}^*$  units and  $1.77 \Delta E_{00}$  units) [31]. Therefore, none of the evaluated IRS would be able to mask discolored substrates, according to ISO [30]. However, when the restorative structures were cemented on tooth-colored substrates, simulating a clinical situation, only YLD-T showed  $\Delta E_{ab}^*$  and  $\Delta E_{00}$  values below AT for all comparisons (ND3–ND8, ND3–ND9 and ND8–ND9) (Table 2 and Fig. 3), meaning, substrate color influenced on the esthetic appearance of resin-bonded IRS, excepted for YLD-T, partially accepting the first study hypothesis.

Notwithstanding, using color difference thresholds (PT and AT) to evaluate masking ability from TP values could present limitations. TP values are dependent on the white and black backgrounds used for color measurements, and it is difficult to obtain perfect white and black backgrounds (as suggested in TP formulation) or having backgrounds with the exact same color coordinates at different research centers. Thus, using a commercially available material designed for dentistry, e.g. tooth-colored resin-based composite, as a substrate, may facilitate future research studies.

Further, it has been reported that CIEDE2000 metric is more effective on showing color differences similar to visual perception than CIELAB metric [39,40]. Previous studies on visual thresholds also showed that CIEDE2000 offered a better fit than CIELAB to evaluate color difference thresholds [31,41]. Yet, the present study did not find significant differences between these two metrics for the materials evaluated. In addition, the parametric factors ( $K_L = 1$ ,  $K_C = 1$ ,  $K_H = 1$ ) for CIEDE2000 color difference metric were set to 1:1:1, since they are currently standardized by CIE [32]. Although, some studies [39,42,43] suggested the use of 2:1:1 instead of 1:1:1. As both versions, 2:1:1 and 1:1:1, showed statistically similar results, only the recommended version (1:1:1) is presented in this report.



**Fig. 3 – Histograms of (a) CIELAB ( $\Delta E_{ab}^*$ ) and (b) CIEDE2000 ( $\Delta E_{00}$ ) color differences between specimens of the same indirect restorative systems (IRS) cemented on different substrates (ND3, ND8 and ND9). The horizontal lines represent perceptibility (PT = 1.22  $\Delta E_{ab}^*$  units and 0.81  $\Delta E_{00}$  units) and acceptability (AT = 2.66  $\Delta E_{ab}^*$  units and 1.77  $\Delta E_{00}$  units) thresholds (Paravina et al. [31]).**

ISO [30] suggests specimen thickness of 1 mm for composites and 0.3 mm for ceramics. As the present study was designed to simulate indirect dental restorations bonded to tooth-colored substrates, a 1.5 mm-thick structures were used.

It is worth mentioning that although all specimens were fabricated from shade A1, there was a wide distribution in CIELAB color coordinates (Fig. 1). This fact was previously studied with different dental ceramics [2]. There are important relationships between chemical composition, microstructure, atomic structure, fabrication process, and properties of dental materials [8]. Such relationships are even more critical for

multilayer IRS, when a complete structural characterization, contemplating each material layer and interface, should be considered. Translucency is one of the main factors involved in dental esthetics and it is critical on selecting dental materials. The IRS evaluated in the present study have different composition, microstructure, crystalline content, phases and layers, which may influence the optical properties of these systems. Thus, significant differences for TP and TP<sub>00</sub> values were found among the evaluated IRS (Fig. 2). However, when the translucency thresholds are used to compare IRS, there were  $\Delta TP$  (0.83 for PICN/LDC; 1.24 for PICN/CAD-on; and 0.41 for LDC/CAD-on) and  $\Delta TP_{00}$  (0.13 for LDC/CAD-

on) values below the translucency perceptibility threshold ( $TPT = 1.33$ ; and  $TPT_{00} = 0.62$ ), and also  $\Delta TP$  (2.93 for LDC/YZW; and 2.52 for YZW/CAD-on) and  $\Delta TP_{00}$  (1.02 for PICN/LDC; 1.15 for PICN/CAD-on; 1.46 for LDC/YZW; and 1.33 for YZW/CAD-on) values below the translucency acceptability threshold ( $TAT = 4.43$ ; and  $TAT_{00} = 2.62$ ) [36]. As CIEDE2000 offers a better data fit than CIELAB metric for translucency thresholds [36], it can be assumed that for common human observers LDC and CAD-on show non-perceptible translucency differences and acceptable translucency differences when compared to PICN and YZW.

LDC, YZW and CAD-on showed acceptable translucency differences, which is probably due to CAD-on structural composition (LDC glass fused to YZW). The present study did not show differences for TP values between LDC and CAD-on, different from a previous study [25], which evaluated different specimen thicknesses and translucencies (LT and HT) of these systems and found that LDC showed greater TP values than CAD-on. Such differences between studies are probably due to the difference on optical properties of the zirconia frameworks (IPS e.max<sup>®</sup> ZirCAD vs Zenostar Zr Translucent). Previous studies showed greater TP values for lithium disilicate-based glass-ceramic than for PICN [44,45], disagreeing from the present study, which is probably due to the comparison between IPS e.max CAD LT and VITA Enamic<sup>®</sup> HT.

The bilayer structure (YLD-T) is composed of a zirconia framework (IPS e.max<sup>®</sup> ZirCAD) and a feldspathic veneer. Despite of the polycrystalline structure (IPS e.max<sup>®</sup> ZirCAD), considered an opaque material [12], has different optical properties (scattering, absorption and transmittance) than human dentin at same thickness (0.5 mm-thick specimens) [46], both of them showed similar TP values [47]. As the zirconia framework and the feldspathic veneer have different refractive indexes (2.1 and 1.55, respectively) [48], when light hits on the bilayer structure, the interaction of light flux through these structures is modified. Thus, the optical phenomena (reflection and scattering) in a multilayer structure could be different [9,49] and more opacity could be found in the restorative system. Additionally, the opaque effect of zirconia is attributed to the grain size, slightly larger than the wavelength of visible light [8,50]. These findings show that translucency varies with structural characteristics, accepting the second study hypothesis.

As a limitation of the present study, only instrumental color measurements were performed. Previous studies recommended [39,40,51] that instrumental shade determination should be accompanied by experienced human visual assessments, which could help to confront the visual thresholds and to have a better perceptive information about the masking ability of indirect restorative systems and clinical acceptability.

## 5. Conclusions

Within the above mentioned limitations of the present *in-vitro* study, it can be stated that resin-cemented YLD-T on different tooth-colored substrates showed less translucency and color

differences below acceptability threshold, indicating the best masking ability among the evaluated systems.

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